# System identification in a historical perspective

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Updated version of

M. Gevers, «A personal view of the development of system identification ...», IEEE Control Systems Magazine, 2006

## Outline

- The origins of system identification
- 1965: the birth of identification in engineering
- The parametric Prediction Error framework
- Search for the model structure: key stumbling block
- Major challenge today: reduce the cost of identification
- Non-parametric approaches
- Reducing the cost of the experiment
- Application-oriented experiment design
- Present research areas
- Conclusions

## The origins of system identification

• The early work in system identification was developed by the statistics and time series communities

- It has its roots in the work of Gauss (1809) and Fisher (1912) and the theory of stochastic processes
- See Deistler (2002) for an excellent survey of this work

## Start the of the model-based control era

1960: Kalman's key papers - start of the state-space era (Kalman:1960a,b)

$$\left\{ egin{array}{rcl} x_{t+1}&=&Ax_t+Bu_t\ y_t&=&Cx_t \end{array} 
ight.$$

• Development of a model-based theory for prediction, filtering and control

- Kalman filter replaces Wiener filter
- Pole placement and LQG control
- Applications initially in areas where good models are available (aerospace, mechanical, electrical systems)

Growing pressure to apply these modern techniques to areas where models are not available from physics

Need for system identification

### Identification in a nutshell

What is system identification ?

Identification is the task of constructing a dynamical model that can predict the outputs of a dynamical system:

Either driven by input and noise:

Or driven by noise only:

System



Predict y(t) from past u(), y() data

Predict y(t) from past y() data only

v(t)

y(t)

w(t)

#### What kind of dynamical models ?

#### State-space models

with measured input:

$$\left\{ egin{array}{rcl} x_{t+1}&=&Ax_t+Bu_t+Ke_t\ y_t&=&Cx_t+e_t \end{array} 
ight.$$

without measured input:

$$\left\{egin{array}{ccc} x_{t+1}&=&Ax_t+Ke_t\ y_t&=&Cx_t+e_t\end{array}
ight.$$

#### Input/output models

with measured input:

$$egin{aligned} y_t + a_1 y_{t-1} + \ldots + a_n y_{t-n} \ &= b_1 u_{t-1} + \ldots + u_{t-m} \ &+ e_t + c_1 e_{t-1} + \ldots + c_p e_{t-p} \end{aligned}$$

without measured input:

$$y_t + a_1 y_{t-1} + \ldots + a_n y_{t-n}$$
  
=  $e_t + c_1 e_{t-1} + \ldots + c_p e_{t-p}$ 

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Identification in the engineering world: The two milestone papers of 1965

• Ho and Kalman (1965), `Effective construction of linear statevariable models from input-output data', *Regelungstechnik,* Vol. 12, pp. 545-548.

Gave birth to realization theory  $\longrightarrow$  subspace identification

• Aström and Bohlin (1965), `Numerical identification of linear dynamic systems from normal operating records', *Proc. IFAC Symp on Self Adaptive Systems, Teddington, UK.* 

Gave birth to Prediction Error Identification (PEI)

### **Realization theory**

How to go from an infinite description of a system

$$H(z) = \sum_{k=1}^{\infty} rac{H_k z^{-k}}{k}$$

to a finite description :

$$H(z) = C(zI - A)^{-1}B$$

 $\{H_1, H_2, H_3, \ldots\} \implies \{A, B, C\} \text{ with } A \in \mathbb{R}^{n \times n}, B \in \mathbb{R}^{n \times m}, C \in \mathbb{R}^{p \times n}$ 

Two aspects :

- find the McMillan degree of  $H(z) \Longrightarrow \dim A$
- find the parameters of A, B, C.

$$y_t = \sum_{k=1}^{\infty} H_k u_{t-k} \quad \Longleftrightarrow \quad \left\{ \begin{array}{ll} x_{t+1} &=& A x_t + B u_t \\ y_t &=& C x_t \end{array} 
ight.$$

### Key tool: the Hankel matrix

$$\mathcal{H} = \begin{bmatrix} H_1 & H_2 & H_3 & H_4 & \dots \\ H_2 & H_3 & H_4 & H_5 & \dots \\ H_3 & H_4 & H_5 & H_6 & \dots \\ \vdots & \vdots & \vdots & \vdots & \end{bmatrix} = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \end{bmatrix} \begin{bmatrix} B & AB & A^2B & \dots \end{bmatrix}$$

If the McMillan degree of H(z) is n, then

1. rank  $\mathcal{H} = n$ 

2.  $\exists A, B, C$  such that  $H_k = CA^{k-1}B$  with  $A \in \mathbb{R}^{n \times n}, B \in \mathbb{R}^{n \times m}, C \in \mathbb{R}^{p \times n}$ 

#### Stochastic realization theory (1970-1975) (Akaike, 1974)

#### Combines realization theory and innovations theory

Given the covariance sequence  $\{R_0, R_1, R_2, ...\}$  of a zero-mean stochastic process  $\{y_t\}$ , where  $R_k \triangleq E\{y_t y_{t-k}^T\}$ , find a minimal Markovian representation for  $\{y_t\}$ :

$$\begin{cases}
x_{t+1} = Ax_t + K\varepsilon_t \\
y_t = Cx_t + \varepsilon_t
\end{cases}$$
(1)

where  $\varepsilon_t$  is a zero-mean white noise sequence, i.e. find the state-space matrices  $\{A, K, C\}$  with n = dim(A) minimal, such that the covariance of the output of (1) is exactly  $R_k$ .

Solution based on the Hankel matrix formed from the  $R_k$ .

Basis for subspace identification, developed much later

## ARMAX, Likelihood function and the Prediction Error framework

Åström and Bohlin (1965)

• Input-output formulation : the ARMAX model structure

 $A(z^{-1})y_t = B(z^{-1})u_t + \lambda C(z^{-1})e_t, \quad \{e_t\}: i.i.d.$ 

- Prediction errors  $\{\varepsilon_t\}$ :  $C(z^{-1})\varepsilon_t = A(z^{-1})y_t B(z^{-1})u_t$
- Likelihood function for a Gaussian p.d.f.:

$$\begin{split} L(\theta) &= -\frac{1}{2\lambda^2} \sum_{t=1}^N \varepsilon_t^2(\theta) - N \log \lambda + \text{constant} \\ \max_{\theta} L(\theta) &\iff \min_{\theta} \frac{1}{2} \sum_{t=1}^N \varepsilon_t^2(\theta) = \min_{\theta} V_N(\theta) \\ \hat{\theta} &= \arg\min_{\theta} V_N(\theta), \quad \hat{\lambda}^2 = \frac{2}{N} V_N(\hat{\theta}) \end{split}$$

•  $\Rightarrow$  adopt  $V(\theta) = \frac{1}{2} \sum_{t=1}^{N} \varepsilon_t^2(\theta)$  as a reasonable criterion even in the absence of a Gaussian probability function: Prediction Error framework; originally suggested by Gauss (1809): see Åström (1980).

## State of the art around 1975

- Two fundamentally different approaches:
  - State-space model: by Hankel matrix factorization. Projection methods. Easy but not optimal. No need for parametrization.
  - I/O model : by minimization of PE criterion. Slower but optimal. Requires choice of model structure. Allows characterization of variance errors through Fisher information matrix.
- After 1975 the parametric (prediction error) approach took over the field.
- Main driving force behind the success of PE methods: Lennart Ljung, and software development (with increased computation speed)
- Hankel matrix approach re-emerged after 1990: subspace state-space methods.

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#### Prediction Error Identification in one slide

- True system  $\mathcal{S}: y_t = G_0(z)u_t + \underbrace{H_0(z)e_t}_{w_t}$
- Model set  $\mathcal{M}: y_t = G(z, heta) u_t + H(z, heta) \epsilon_t$
- Model  $\Leftrightarrow$  predictor:  $\hat{y}_{t|t-1}(\theta) = H^{-1}(z,\theta)G(z,\theta)u_t + (1 H^{-1}(z,\theta))y_t$
- Prediction error:  $arepsilon_t( heta) = y_t \hat{y}_{t|t-1}( heta)$
- Criterion  $V_N( heta,Z^N) = rac{1}{N}\sum_{t=1}^N ||arepsilon_t( heta)||^2$
- The parameter estimate:  $\hat{\theta}_N = \arg \min_{\theta \in \mathcal{D}_{\theta}} V_N(\theta, Z^N)$
- Transfer function estimates:  $G(z, \hat{\theta}_N), H(z, \hat{\theta}_N)$
- If  $\exists \theta_0 : G(z, \theta_0) = G_0(z)$  and  $H(z, \theta_0) = H_0(z)$ , then:

$$\sqrt{N}(\hat{ heta}_N- heta_0) \stackrel{N
ightarrow\infty}{\longrightarrow} N(0,P_ heta)$$



### Key new concept: identification as a design problem (1986) (Gevers&Ljung,1986; Wahlberg&Ljung,1986)

### Basic observation:

every model is at best an approximation of the exact system it contains errors

## Two aspects:

- Model structure and criterion should be tuned towards the application of the model
- Experiment should be tuned towards the application criterion

Prediction Error Identification is well suited to this design view

### Example

When a system  $y_t = G_0(z)u_t + v_t$  is modeled by a model structure  $y_t = G(z, \theta)u_t + \epsilon_t$ , the PE criterion minimizes

$$\hat{\theta}_N \to \arg\min V(\theta) = \frac{1}{2\pi} \int_{-\pi}^{\pi} \left\{ \mid G(e^{j\omega}, \theta) - G_0(e^{j\omega}) \mid^2 \Phi_u(\omega) + \Phi_v(\omega) \right\} d\omega$$

 $\implies$  If the application is to have a good model in a narrow bandwidth defined by a bandpass filter  $W(e^{j\omega})$ , then open loop identification with an input spectrum  $\Phi_u(\omega) = |W(e^{j\omega})|^2 \Phi_v(\omega)$  will meet that objective.

## 1965 - 2000: what had been accomplished?

- Both approaches have been developed:
  - \* Parametric Prediction Error approach
  - \* Non-parametric state-space (subspace) approach
- A frequency domain approach has been developed, showing advantages of periodic excitation
- Theory is for the most part well understood
- Field of applications have been enormously widened
- Model Predictive Control has become the standard for most control applications
- Progress in nonlinear system identification

## **Bottlenecks and limitations**

- Modeling and identification is still the most costly part of any advanced control design
- Model building accounts for 50% to 75% of total cost in an advanced control project
- Major bottleneck: search for the best model structure
- Prediction error criterion is non-convex: problem of local minima
- Identification of MIMO systems is still a difficult task
- Nonlinear identification is still in its infancy
- Identification of structured systems (e.g. distributed and networked control systems)

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#### Key stumbling block in PE identification: choice of model structure



#### Illustration (courtesy Pintelon, Schoukens, Ljung)

7000 data are generated by a «true» BJ system:

$$y_t = \frac{0.0947 + 0.2463z^{-1} + 0.0947z^{-2}}{1 - 0.5376z^{-1} + 0.7357z^{-2}}u_t + \frac{1 + 0.776z^{-1}}{1 - 0.1584z^{-1}}e_t$$

Apply the standard procedure of the Matlab SI toolbox:

- Split data set into two (estimation and validation data set)
- Estimate delay: d=0
- Initial guess with N4SID: yields state-space model m3 of order 3
- Compare with state-space models of order 1 and 2: m1 and m2
- Fits on validated data:
  - ➡ m1: 57.6 % fit
  - ➡ m2: 86.1 % fit
  - ➡ m3: 87.1 % fit

Fit = part of the output variation that is explained by the model

#### Analysis of model m3:



#### Conclusion of the analysis

- Common poles and zeros in I/O and noise model
- Eliminate common poles and zeroes and try BJ model of order 2
- This yields an estimated model with fit 87.2%

$$y_t = \frac{0.0902 + 0.2493z^{-1} + 0.0912z^{-2}}{1 - 0.5377z^{-1} + 0.7357z^{-2}}u_t + \frac{1 + 0.9726z^{-1}}{1 - 0.1579z^{-1}}e_t$$



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Major goal of present research: reducing the cost of the identification

What is the cost of modeling and identification?

1. Man-hour costs



- Reduce human intervention, particularly expert intervention. User-friendly identification.
- 2. Cost of the experiment



Reduce experiment time and performance degradation during data collection.

Optimal experiment design.

- 3. Cost of estimating useless system properties
  - Cost of complexity.

Application-oriented experiment design

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## Steps towards user-friendly identification

## Main idea:

- first compute a nonparametric estimate of the system and noise distribution
- use these as a starting point for more efficient parametric PE identification

## Two possible strategies:

- state-space subspace identification
  - ★ CVA (Larimore, 1990, 1996)
  - ★ N4SID (Van Overschee and De Moor, 1994)
  - ★ MOESP (Verhaegen, 1994)
- nonparametric frequency domain identification

(VUB group: Pintelon, Schoukens, Rolain, Vandersteen, et al.)

### Key step in the subspace methods

• An estimate of the Hankel matrix of impulse responses is obtained from I/O data.

• Recall the basic tool  $y(t) = \sum_{k=1}^{\infty} \ H_k \ u(t-k)$ 

$$\mathcal{H} = \begin{bmatrix} H_1 & H_2 & H_3 & H_4 & \dots \\ H_2 & H_3 & H_4 & H_5 & \dots \\ H_3 & H_4 & H_5 & H_6 & \dots \\ \vdots & \vdots & \vdots & \vdots & \end{bmatrix} = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \end{bmatrix} \begin{bmatrix} B & AB & A^2B & \dots \end{bmatrix}$$

- Perform an SVD of the Hankel matrix
- Truncate by deleting all singular values below some threshold
- This fixes the order of the state space system, i.e. size of A
- A second LS step is needed to compute the remaining matrices

Estimation of the Frequency Response Function  $\hat{G}(e^{j\omega})$ 

Time versus frequency domain identification

System and noise model:

$$y(t) = G_0(z)u(t) + v(t) = G_0(z)u(t) + H_0(z)e(t)$$

Time domain PE criterion:

$$V_N( heta) = rac{1}{N} \sum_{t=1}^N \left( H^{-1}(z, heta) [y(t) - G(z, heta) u(t)] 
ight)^2$$

Frequency domain PE criterion:

$$\begin{split} V_{N}(\theta) &= \frac{1}{N} \sum_{k=-\frac{N}{2}+1}^{\frac{N}{2}} \left( H^{-1}(k,\theta) [Y(k) - G(k,\theta)U(k)] \right)^{2} \\ \text{where } G(k,\theta) &= G(e^{j2\pi k/N}), \ H(k,\theta) = H(e^{j2\pi k/N}) \text{ and} \\ X(k) &= \frac{1}{\sqrt{N}} \sum_{t=0}^{N-1} x(t) e^{-j2\pi kt/N} = \text{DFT of } x(t) \end{split}$$

#### Precise frequency domain formulation

For a finite record  $t = 0, \ldots, N - 1$ :

$$y(t) = G_0(q)u(t) + t_G(t) + H_0(q)e(t) + t_H(t).$$

Frequency domain formulation:

$$Y(k) = G_0(\Omega_k)U(k) + T_G(\Omega_k) + H_0(\Omega_k)E(k) + T_H(\Omega_k)$$
  
=  $G_0(\Omega_k)U(k) + H_0(\Omega_k)E(k) + \underbrace{T(\Omega_k)}_{\text{leakage term}}$ 

Frequency domain criterion becomes:

$$V_N( heta) = rac{1}{N} \sum_{k=-rac{N}{2}+1}^{rac{N}{2}} \left( H_k^{-1}( heta) [Y(k) - G_k( heta) U(k) - T_k( heta)] 
ight)^2$$
  
where  $G_k( heta) riangleq G(\Omega_k, heta), \ H_k( heta) riangleq H(\Omega_k, heta), \ T_k( heta) riangleq T(\Omega_k)$ 

#### The Local Polynomial Method (LPM)

(VUB group: Schoukens, Pintelon, Barbé, Rolain, Vandersteen, 2009)

$$Y(k) = G_0(\Omega_k)U(k) + H_0(\Omega_k)E(k) + \underbrace{T(\Omega_k)}_{\text{leakage term}}$$

Observation:  $G_0(\Omega_k)$  and  $T(\Omega_k)$  are smooth rational functions.

$$egin{aligned} G_0(\Omega_{k+r}) &pprox & G_0(\Omega_k) + \sum_{s=1}^R g_s(k) r^s, \ T_0(\Omega_{k+r}) &pprox & T_0(\Omega_k) + \sum_{s=1}^R t_s(k) r^s, \ ext{for } r = \mathbf{0}, \pm \mathbf{1}, \dots, \pm n \end{aligned}$$

Define

$$egin{aligned} heta_k & riangleq \left[G_0(\Omega_k) \; g_1(k) \ldots \; g_R(k); T_0(\Omega_k) \; t_1(k) \ldots \; t_R(k)
ight]^T \end{aligned}$$

We can estimate  $heta_k$ ,  $k = 1, \ldots, N$  from local measurements

$$\{U(k-n),\ldots,U(k),\ldots,U(k+n); \hspace{0.2cm} Y(k-n),\ldots,Y(k),\ldots,Y(k+n)\}$$

over a local frequency window of size 2n around  $\Omega_k$ .

#### Benefits of the Local Polynomial Method (LPM)

- Excellent nonparametric estimate of  $\widehat{G}(\Omega_k)$
- Plus nonparametric estimate of  $\widehat{T}(\Omega_k)$ , and of  $\widehat{\Phi}_v(\Omega_k)$  from residuals
- Requires little or no expert user intervention
- Both are very useful starting points for parametric estimates
  - $\ast \ \widehat{G}(\Omega)$  gives good idea of what  $G_0(\Omega)$  looks like
  - \*  $\widehat{\Phi}_v(\Omega_k)$  can be used to simplify the criterion for estimation of  $G(\Omega, \theta)$ :

$$V_N( heta) = rac{1}{N} \sum_{k=-rac{N}{2}+1}^{rac{N}{2}} rac{\left[Y(k) - G_k( heta)U(k) - \widehat{T}(\Omega_k)
ight]^2}{\widehat{\Phi}_v(\Omega_k)}$$

• Risk of local minima with the latter criterion is greatly reduced (Schoukens et al; CDC-ECC2011)

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## Least costly identification for robust control

### Classical design:

Minimize a measure of the uncertainty subject to constraints

#### Dual idea:

Minimize the identification cost subject to a required quality

### Cheapest cost:

Can be the length of the experiment, the applied signal energy, or the perturbation cost.





Bombois, Scorletti, Gevers, Van den Hof, Hildebrand, 2004-2006

The dual approach to experiment design Illustration with open loop design

## Classical approach:

 $\min_{\Phi_u(\omega)} \det(P_{\theta}) \text{ or } \\ \min_{\Phi_u(\omega)} \int_{-\pi}^{\pi} Var\{G(e^{j\omega}, \hat{\theta}_N)\}d\omega \} \text{ subject to } \int_{-\pi}^{\pi} \Phi_u(\omega)d\omega \leq \alpha$ 

## Dual approach:

$$\min_{\Phi_u(\omega)} \int_{-\pi}^{\pi} \Phi_u(\omega) d\omega \text{ subject to} \begin{cases} \int_{-\pi}^{\pi} Var\{G(e^{j\omega}, \hat{\theta}_N)\} \leq \gamma \text{ or} \\ \\ \int_{-\pi}^{\pi} Var\{C(G(e^{j\omega}, \hat{\theta}_N))\} \leq \gamma \end{cases}$$

#### Application to least costly experiment design

Disturbance rejection problem

Normal operation:



$$egin{array}{l} y_t = G_0(z) u_t + v_t \ u_t = -C(z) y_t \end{array} 
ight
angle \Leftrightarrow y_t = rac{1}{1+C(z)G_0(z)} v_t = S(z) v_t$$

During identification, an excitation signal  $r_t$  is added:

$$y_t = S(z)v_t + \underbrace{G_0(z)S(z)r_t}_{y^r}$$
$$u_t = -C(z)S(z)v_t + \underbrace{S(z)r_t}_{u^r}$$

 $\implies$  Performance degradation cost due to  $y^r$  and  $u^r$ :

$$egin{array}{rl} \mathcal{J}_r &=& \displaystylerac{N}{2\pi} \int_{-\pi}^{\pi} \left( lpha_y \Phi_{y_r} + lpha_u \Phi_{u_r} 
ight) d\omega \ &=& \displaystylerac{N}{2\pi} \int_{-\pi}^{\pi} \left( lpha_y |G_0(e^{j\omega}) S(e^{j\omega})|^2 + lpha_u |S(e^{j\omega})|^2 
ight) \Phi_r(\omega) \; d\omega \end{array}$$

$$\min_{N,\Phi_r(\omega)}\mathcal{J}_r \;\; \text{subject to} \;\; ||\frac{W(z)}{1+C(G(\theta))G(\theta)}||_\infty \leq \gamma \;\; \forall \theta \in \mathcal{D}(\hat{\theta}_N,P_\theta)$$

## But is it all worth the effort?

Illustration with Landau's flexible transmission system (Bombois, Scorletti, 2012)

Experiment design objective

Perform closed-loop identification with fixed controller  $C_{id}$  while

• minimizing performance degradation  $J_r$  due to external  $\Phi_r(\omega)$ :

 $J_r = \beta_u Var\{u_r\} + \beta_y Var\{y_r\}$ 

• maintaining accuracy required by robust control objective:

 $|G_0(e^{j\omega}) - G(e^{j\omega}, \hat{ heta}_N)| \leq r_{adm}(\omega) \hspace{0.2cm} orall \omega \hspace{0.2cm}$  w.p. 95%

Purpose: use this model to design a better controller



- *G*<sub>*init*</sub> does not satisfy quality constraint for robust control design
- but will be used to compute an optimal  $\Phi_r(\omega)$

Step 2: computation of closed-loop optimal experiment

 $G_{init}$  is used to solve the closed-loop optimal design problem.

Two suboptimal solutions for  $\Phi_r(\omega)$  are sought:

- white noise:  $\Phi_r(\omega) = \text{constant}$
- $\Phi_{r,10}(\omega) = \sum_{k=-10}^{10} c_k \ e^{j\omega k} \ge 0$

Closed-loop identification (500 data) with these 2 suboptimal spectra:

- with white noise:  $\Rightarrow J_r = 22$
- with optimal  $\Phi_{r,10}(\omega)$ :  $\Rightarrow J_r = 9.3$

We note that the performance degradation induced by the (sub) optimal excitation signal is more than two times smaller than with white noise excitation

#### Some comparisons:



Alternatively, the (sub)optimal excitation allows us to achieve the same required accuracy in a much shorter time

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#### Basic concepts (Hjalmarsson, ECC 09 plenary)

#### A. Waterbed effect - fundamental limitation (Rojas, Welsh, Agüero, 2009)

For open loop identification with OE model:

$$rac{1}{2\pi}\int_{-\pi}^{\pi}N\Phi_u(\omega)Var\{G(e^{j\omega},\hat{ heta}_N)\}d\omega=n_G~\sigma_e^2$$

Discussion:

- Energy cost for open loop identification is  $\int_{-\pi}^{\pi} N \Phi_u(\omega) d\omega$
- Requiring low variance everywhere is expensive
- Cost is proportional to number of parameters and to noise variance
- To get  $Var\{G(e^{j\omega}, \hat{ heta}_N)\} \leq rac{1}{\gamma} \;\; orall \omega$  requires  $NE[u^2(t)] \geq \gamma n_G \sigma_e^2$ .

• 
$$\sup_{\omega} Var\{G(e^{j\omega}, \hat{\theta}_N)\} \geq \frac{n_G \sigma_e^2}{NE[u^2(t)]}$$

•  $\Rightarrow$  Do not waste your energy at frequencies where you do not need it !!

## B. Performance degradation and acceptable models (Gevers & Ljung, 1986; Hjalmarsson, 2009)

- Let  ${\mathcal J}$  be the quantity of interest for the application
- With true system:  $\mathcal{J}(S_0)$ ; with a model:  $\mathcal{J}(M(\theta))$ . Assume  $M(\theta_0) = S_0$ .
- Performance degradation measure: differentiable function  $V_{app}(\theta) = ||\mathcal{J}(M(\theta)) - \mathcal{J}(S_0)||$  such that  $V_{app}(\theta_0) = 0$ .
- Set of acceptable models for the application:

$$\mathcal{D}_{app} riangleq \left\{ heta \ : V_{app}( heta) \leq rac{1}{\gamma} 
ight\} \quad (\gamma ext{= accuracy})$$

Example 1: step response application

With true  $\theta_0 : y_t(\theta_0), t = 1, \dots, N$ With estimated  $\hat{\theta}_N : y_t(\hat{\theta}_N), t = 1, \dots, N$  $\Rightarrow V_{app}(\theta) = \frac{1}{N} \sum_{t=1}^N [y_t(\theta_0) - y_t(\hat{\theta}_N)]^2$ 

Example 2: steady-state gain for FIR(n) system

$$\Rightarrow V_{app}( heta) = [\sum_{t=1}^{n} heta_k^0 - \sum_{t=1}^{n} \hat{ heta}_k]^2$$

#### C. Identification uncertainty set

- Define identification criterion and assume system is in model set:
- $V_{id}(\theta) \triangleq \frac{1}{2} \{ E[\epsilon_t(\theta)]^2 \sigma_e^2 \}$ . Note that  $V_{id}(\theta_0) = 0$ .
- $V_{id}(\theta) \approx (\theta \theta_0)^T I(\theta_0)(\theta \theta_0)$  defines ellipsoid
- With probability  $\alpha$ ,  $\hat{\theta}_N \in \mathcal{D}_{id}$  (identification uncertainty set):

 $\mathcal{D}_{id} = ig\{ heta: NV_{id}( heta) \leq \sigma_e^2 \chi_lpha^2(n_ heta)ig\}$  where  $n_ heta = \#$  parameters

• 
$$\chi^2_{\alpha}(n) \approx (\beta + \sqrt{n})^2 = O(n)$$

#### D. Identification with minimal cost

In open loop:  $\min_{N, \Phi_u(\omega)} \int_{-\pi}^{\pi} N \Phi_u(\omega) d\omega$  such that  $\mathcal{D}_{id} \subseteq \mathcal{D}_{app}$ 

#### Interpretation of $\mathcal{D}_{id} \subseteq \mathcal{D}_{app}$

Let  $V_{app}(\theta)$  be three times differentiable. Then:

$$\mathcal{D}_{app} ~pprox \left\{ heta ~:~ \gamma( heta- heta_0)^T V_{app}^{''}( heta_0)( heta- heta_0) \leq 1 
ight\}$$

while

$$\mathcal{D}_{id} ~~pprox ~~ \left\{ heta : rac{N}{\sigma_e^2 \chi_lpha^2(n_ heta)} ( heta - heta_0)^T I( heta_0) ( heta - heta_0) \leq 1 
ight\}$$

Therefore:

$$\mathcal{D}_{id} \subseteq \mathcal{D}_{app} \iff \underbrace{\underbrace{N.I(\theta_0)}_{id} \geq \gamma.\sigma_e^2.\chi_{\alpha}^2(n_{\theta}).V_{app}^{''}(\theta_0)}_{identification effort:}$$
  
identification effort:  
data length x information matrix

Application-oriented experiment design

$$\mathcal{D}_{id} \subseteq \mathcal{D}_{app} \iff \overbrace{\underbrace{N.I( heta_0)}_{I} \geq \gamma.\sigma_e^2.\chi^2_{lpha}(n_{ heta}).V^{''}_{app}( heta_0)}$$

identification effort: data length x information matrix

If  $V_{app}^{''}(\theta_0)$  is singular, of rank  $m < n_{\theta}$ , then  $I(\theta_0)$  can be singular and  $\chi^2_{\alpha}(n_{\theta})$  replaced by  $\chi^2_{\alpha}(m) \Longrightarrow$  identification cost is reduced.

#### Example: estimation of steady state gain of FIR(n) system

- $y_t = \sum_{k=0}^{n-1} heta_k u_{t-k} + e_t$
- Compare white noise input u with variance  $\sigma_u^2$  with constant input  $u_t = \sigma_u$ .
- With constant input, same precision is obtained with n times less input energy (ex: required data length is n times smaller)

See also Mårtensson and Hjålmarsson, 2011



## Outline

- The origins of system identification
- 1965: the birth of identification in engineering
- The parametric Prediction Error framework
- Search for the model structure: key stumbling block
- Major challenge today: reduce the cost of identification
- Non-parametric approaches
- Reducing the cost of the experiment
- Application-oriented experiment design
- Present research areas
- Conclusions

## Active research areas

They can be broadly classified in two categories

#### 1. Improving the quality of the estimate

- Regularization methods, Bayesian methods
- Minimizing the Mean Square Error
- Bias-variance trade-off
- Optimal model order selection

#### 2. Experiment design questions

- Optimal experiment design
  - ✦ Open loop, closed loop, joint closed loop design
  - Linear systems and nonlinear systems
  - Parametrization of all input spectra
- Informative experiments and identifiability
  - + For networks of dynamical systems
  - + For classes of nonlinear models

### 1. Regularisation, Bayesian estimation and kernel methods

Connects «classical» system identification with machine learning and Bayesian estimation.

Simple introduction: consider a linear regression model

 $Y_N = \Phi_N \theta + V_N$ 

Least squares estimate:

 $\hat{\theta} = \arg\min_{\theta} ||Y_N - \Phi_N \theta||^2 = (\Phi_N^T \Phi_N)^{-1} Y_N$ 

 $\Phi_N^T \Phi_N$  may be singular or ill-conditioned  $\implies$  add **regularization term**:

$$egin{argmin} \hat{ heta} &= rgmin_{ heta} ||Y_N - \Phi_N heta ||^2 + \gamma heta^T P^{-1} heta \ &= P \Phi^T (\Phi P \Phi + \gamma I)^{-1} Y_N \end{split}$$

### Regularisation, Bayesian estimation, kernel methods (cont'd)

Much present research is on the search for the best regularization term and on the interpretation: see the excellent survey paper Pillonetto, Dinuzzo, Chen, De Nicolao, Ljung, 2014

• Kernel-based approach: function estimation in infinite-dimensional space with added regularization term. Introduced into system identification by Pillonetto and De Nicolao, 2010

• Empirical Bayes approach: impulse response is modeled as a zero-mean Gaussian process; the parameters of the pdf are estimated by Max Likelihood: Rasmussen and Williams, 2006

• This idea was first proposed in the stochastic embedding approach: Goodwin, Gevers, Ninness, 1992. Connection is established in Ljung, Goodwin, Aguero, 2014

A key element of the discussion is the model order selection problem which is closely linked to the bias-variance tradeoff.

#### 2. Optimal experiment design questions

Key references for optimal experiment design: Goodwin & Payne, 1977; Zarrop, 1979

Joint optimal experiment design problem for closed-loop linear systems:

 $\min_{C_{id}(z), \ \Phi_r(\omega)} J,$  where J can be

• quality criterion. Ex:  $J = \int_{-\pi}^{\pi} Var(C(\hat{G}_N(\omega)))d\omega$  or  $Var(\hat{G}) < \gamma(\omega) \quad \forall \omega$ • or cost criterion. Ex:  $J = \int_{-\pi}^{\pi} \Phi_r(\omega)d\omega$ 

 $C_{id}$ 

 $v_t$ 

 $G_0$ 

Always subject to constraints.

Examples:  $\int_{-\pi}^{\pi} \Phi_y(\omega) d\omega \leq \alpha$ , or  $|\Phi_y(\omega)| \leq \alpha \ \forall \omega$ 

Optimal solution for integral criteria and integral constraints only: Hildebrand, Gevers, Solari, 2014

Solution over a restricted set of spectra for integral and pointwise constraints: Hjalmarsson & Jansson, 2008 Open loop design for classes of nonlinear systems

Optimal input design for nonlinear systems is very hard.

Optimal or suboptimal solutions are obtained by

- restricting the class of model structures
- ✦ restricting the class of inputs

Example:

• Model class: Nonlinear FIR

$$y_t( heta) = G_{NL}(u_t, u_{t-1}, \dots, u_{t-n+1}, heta)$$

• Input signal: finite set of possible values

$$u_t \in \{u_1, \dots, u_A\}$$

Larsson, Hjalmarsson and Rojas, 2010; De Cock, Gevers, Schoukens, 2014

#### Parametrization of all input spectra yielding the same covariance

Consider open loop identification and an OE model structure:

 $y_t = G(z, \theta)u_t + e_t$  with  $\dim(\theta) = n$ 

Then the normalized asymptotic covariance matrix of  $\hat{\theta}_N$  can be written as

$$P_{\theta}^{-1} = \frac{1}{2\pi} \int_{-\pi}^{\pi} \left( \frac{\partial G(e^{j\omega}, \theta)}{\partial \theta} \right) \left( \frac{\partial G(e^{j\omega}, \theta)}{\partial \theta} \right)^* \Phi_{\boldsymbol{u}}(\boldsymbol{\omega}) d\boldsymbol{\omega} + M_e$$

Then the set of all achievable  $P_{\theta}$  (for all possible  $\Phi_u(\omega)$ ) can be parametrized as a linear combination of *n* matrices:

 $P_{\theta}^{-1} = m_1 R_1 + \ldots + m_n R_n + M_e$ 

This gives a parametrization of all spectra yielding the same covariance  $P_{\theta}$ .

Mahata, 2013

## 3. Informative experiments and identifiability

#### Identification of dynamic systems within networks



- $w_j$ : measured
- $v_j$ : unmeasured

All kinds of interesting questions, that can be summed up as:

• Identifiability and experiment design questions: Example: which signals do I need to identify  $G_{21}^0$ ? Answer:  $w_1$  and  $w_2$  suffice

• Accuracy questions:

Example: do I get a better estimate of  $G_{21}^0$  if I also measure  $w_3$ ? Answer: yes, by simultaneously estimating  $G_{21}^0$  and  $G_{23}^0$ .

Van den Hof, Dankers, Heuberger, Bombois, 2013, 2014

Identifiability and informativity for nonlinear systems

• For the very broad model class

 $\dot{x} = f(x,u, heta), \quad y = h(x,u, heta)$ 

Sufficient conditions for identifiability of  $\theta$ based on application of the Ritt algorithm: Ljung and Glad, 1994 Powerful but huge computational requirements.

• For nonlinear model classes that are affine in  $\theta$ Recent results on identifiability and informative experiments:

Gevers, Bazanella, Coutinho, Dasgupta, 2014

## Conclusions

- ✤ System identification in engineering started almost 50 years ago
- Enormous progress has been accomplished
- It is still the major task in any advanced control project
- Major challenge today: reduce the cost of identification
  - Make it more user friendly and data-driven
  - Optimize the experiment: less time, less energy
  - Tune the experiment towards the application: don't waste !
- Many research challenges remain, new ones have appeared:
  - Structured systems
  - Nonlinear systems
  - Large distributed and network controlled systems

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