

Model Reduction of Dynamical Systems

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Motivation

Predict a storm surge in the North sea (Verlaan-Heemink '97)

60.000 variables, 15 inputs (buoys and radars)

Problem

Using measurements predict the state of the North Sea variables in order to operate the sluices in due time (6h.)

Solution

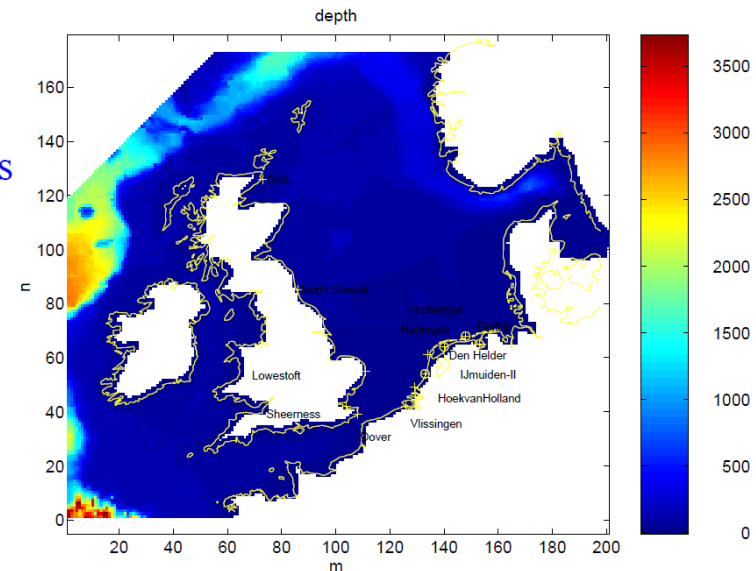
$x(t) \doteq [h(t), v_x(t), v_y(t)]$ satisfies the shallow water equations

$$\partial x(t)/\partial t = F(x(t), w(t))$$

$$y(t) = G(x(t), v(t))$$

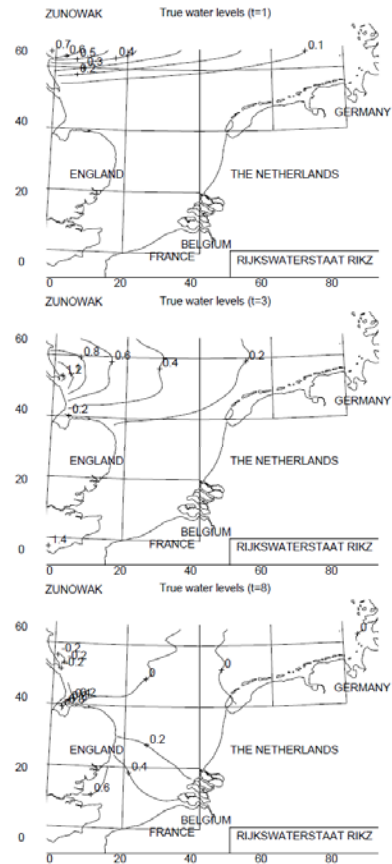
with measurements $y(t)$ and noise processes $v(\cdot), w(\cdot)$

\Rightarrow estimate and predict $\hat{x}(t)$ using Kalman filtering

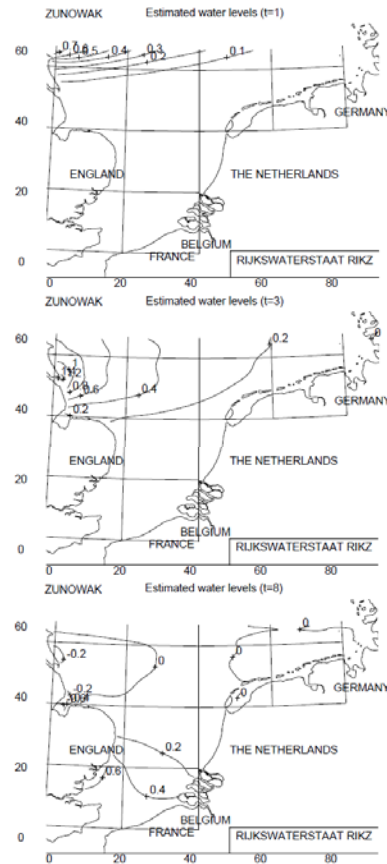


Motivation

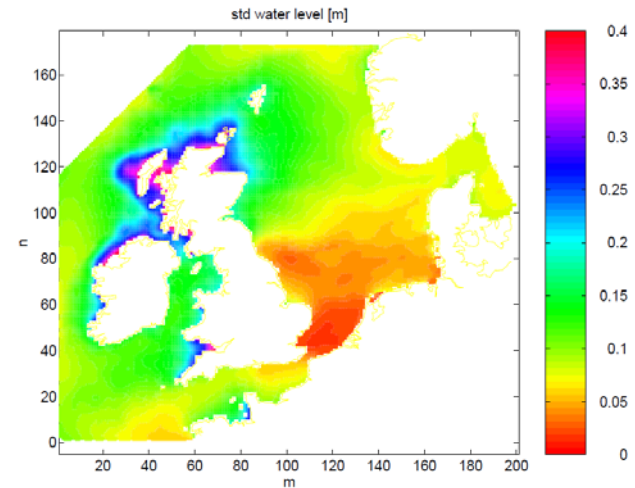
True water levels



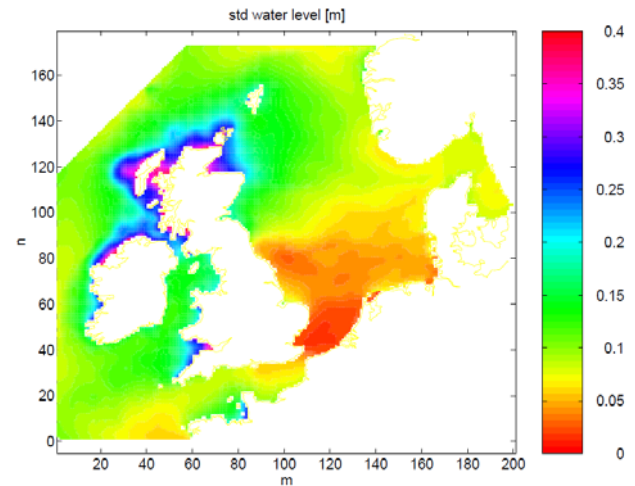
Estimated water levels



Reconstruction works well around estuarium



Standard deviation of fi lter using 8 measurement locations



Standard deviation of fi lter using measurement locations
(1 used for validation)

What models ?

General implicit dynamical systems are modeled via

$$\mathcal{S} \left\{ \begin{array}{l} F(\dot{x}(\cdot), x(\cdot), u(\cdot)) = 0 \\ y(\cdot) = G(x(\cdot), u(\cdot)), \end{array} \right.$$

using “state” $x(\cdot)$ of dimension $N \gg m, p$.

We focus on *explicit* state equations because derivations are simpler

What models ?

continuous-time

$$\begin{cases} \dot{x}(t) = F(x(t), u(t)) \\ y(t) = G(x(t), u(t)) \end{cases}$$

\Downarrow

$$\begin{cases} \dot{x}(t) = A(t)x(t) + B(t)u(t) \\ y(t) = C(t)x(t) + D(t)u(t) \end{cases}$$

\Downarrow

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases}$$

discrete-time

$$\begin{cases} x(k+1) = F(x(k), u(k)) \\ y(k) = G(x(k), u(k)) \end{cases}$$

\Downarrow

$$\begin{cases} x(k+1) = A(k)x(k) + B(k)u(k) \\ y(k) = C(k)x(k) + D(k)u(k) \end{cases}$$

\Downarrow

$$\begin{cases} x(k+1) = Ax(k) + Bu(k) \\ y(k) = Cx(k) + Du(k) \end{cases}$$

The strongest results are for the linear cases

Many results also extend to the implicit case

Some results extend to the time-varying case

Explicit Discrete Linear Time Invariant Systems

$$\begin{cases} x_{k+1} = Ax_k + Bu_k \\ y_k = Cx_k + Du_k, \end{cases}$$

$u_k \in \mathbb{R}^m$, $y_k \in \mathbb{R}^p$, $x_k \in \mathbb{R}^N$, $N \gg m, p$

Find another system driven with the same input $u_k \in \mathbb{R}^m$

$$\begin{cases} \hat{x}_{k+1} = \hat{A}\hat{x}_k + \hat{B}u_k \\ \hat{y}_k = \hat{C}\hat{x}_k + \hat{D}u_k, \end{cases}$$

but with different $\hat{y}_k \in \mathbb{R}^p$, $\hat{x}_k \in \mathbb{R}^n$.

Model reduction = find a model of order $n \ll N$ with small output error $\|y_k - \hat{y}_k\|_{l_2}$ (nearby time responses !)

What norm ?

Transfer functions and norms

$$H(z) = C(zI_N - A)^{-1}B + D, \quad \hat{H}(z) = \hat{C}(zI_n - \hat{A})^{-1}\hat{B} + \hat{D},$$

Take the Fourier transform of the time series (preserves energy)

$$u_f(e^{j\omega}) = \mathcal{F}\{u_k\}, \quad y_f(e^{j\omega}) = \mathcal{F}\{y_k\}, \quad \hat{y}_f(e^{j\omega}) = \mathcal{F}\{\hat{y}_k\}$$

which yields

$$y_f(e^{j\omega}) = H(e^{j\omega})u_f(e^{j\omega}), \quad \hat{y}_f(e^{j\omega}) = \hat{H}(e^{j\omega})u_f(e^{j\omega}).$$

What norm ?

... and hence a bound for $e_k \doteq [y_k - \hat{y}_k]$:

$$\mathcal{F}\{e_k\} = e_f(e^{j\omega}) = [H(e^{j\omega}) - \hat{H}(e^{j\omega})]u_f(e^{j\omega}).$$

Worst case relative error $\frac{\|e_f(e^{j\omega})\|_{l_2}}{\|u_f(e^{j\omega})\|_{l_2}} = \frac{\|y_k - \hat{y}_k\|_{l_2}}{\|u_k\|_{l_2}}$ is bounded by

$$\|H(\cdot) - \hat{H}(\cdot)\|_{\infty} \doteq \sup_{\omega} \|H(e^{j\omega}) - \hat{H}(e^{j\omega})\|_2,$$

Problem : *find the best (stable) approximation $\hat{H}(\cdot)$ of degree n for $H(\cdot)$ in $\|\cdot\|_{\infty}$ norm.*

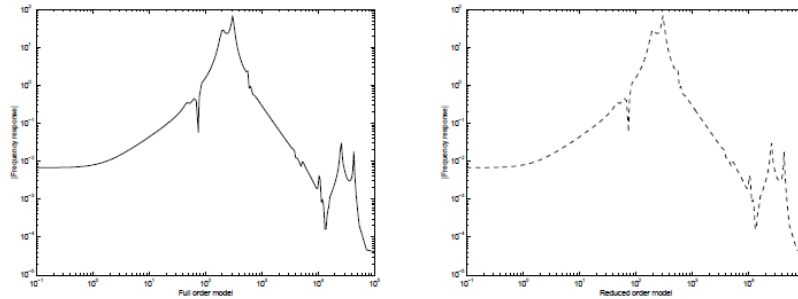
In continuous-time :

Transfer functions and norms

$$H(s) = C(sI_N - A)^{-1}B + D, \quad \hat{H}(s) = \hat{C}(sI_n - \hat{A})^{-1}\hat{B} + \hat{D},$$

are $p \times m$ rational matrices

try to match frequency responses



by minimizing their difference using

$$\|H(\cdot) - \hat{H}(\cdot)\|_{\infty} \doteq \sup_{\omega} \sigma_{\max}\{H(j\omega) - \hat{H}(j\omega)\}$$

Convolution map \mathcal{S} from inputs to outputs

Define $H(z) = H_0 + H_1 z^{-1} + H_2 z^{-2} + \dots$ to find

$$\begin{bmatrix} \vdots \\ y_{-2} \\ y_{-1} \\ y_0 \\ y_1 \\ \vdots \end{bmatrix} = \underbrace{\begin{bmatrix} \ddots & & & & \\ & H_0 & & & \\ & H_1 & H_0 & & \\ & H_2 & H_1 & H_0 & \\ & H_3 & H_2 & H_1 & H_0 \\ & & & \ddots & \end{bmatrix}}_{\mathcal{S}} \begin{bmatrix} \vdots \\ u_{-2} \\ u_{-1} \\ u_0 \\ u_1 \\ \vdots \end{bmatrix}$$

$$\|H(\cdot) - \hat{H}(\cdot)\|_{\infty} = \|\mathcal{S} - \hat{\mathcal{S}}\|_2,$$

\mathcal{S} does not have a discrete set of singular values !

Hankel map H : past inputs to future outputs

Put $u_0, u_1, u_2 \dots = 0$ to see the constrained map

$$\begin{bmatrix} \vdots \\ y_{-2} \\ y_{-1} \\ \hline y_0 \\ y_1 \\ \vdots \end{bmatrix} = \begin{bmatrix} \ddots & & & & \\ & H_0 & & & \\ & H_1 & H_0 & & \\ \hline & \color{red}{H_2} & \color{red}{H_1} & H_0 & \\ & \color{red}{H_3} & \color{red}{H_2} & H_1 & H_0 \\ & & & \ddots & \end{bmatrix} \begin{bmatrix} \vdots \\ \color{red}{u_{-2}} \\ \color{red}{u_{-1}} \\ \hline 0 \\ 0 \\ \vdots \end{bmatrix}$$

$$\|\mathcal{S} - \hat{\mathcal{S}}\|_{\mathcal{H}} = \|\mathcal{H} - \hat{\mathcal{H}}\|_2,$$

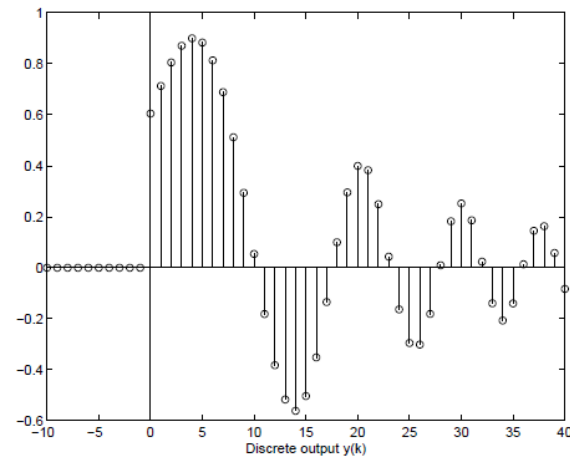
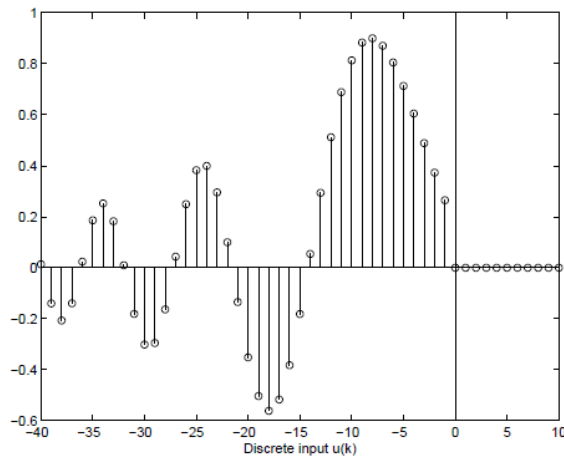
\mathcal{H} has rank N and has discrete singular values !

Hankel map H : past inputs to future outputs

Assume $H_0 \doteq D = 0$ and use identities $H_k \doteq CA^{k-1}B$

$$y_k = \sum_{-\infty}^0 CA^{(k-j)}Bu(j-1) = CA^k \cdot \sum_0^{\infty} A^j Bu(-j-1),$$

$$y_k = CA^k x(0), \quad x(0) = \sum_0^{\infty} A^j Bu(-j-1).$$



$$u_k, \quad k \in (-\infty, 0) \implies x(0) \implies y_k, \quad k \in [0, \infty)$$

Hankel map factorization

$$\begin{bmatrix} y_0 \\ y_1 \\ y_2 \\ \vdots \end{bmatrix} = \underbrace{\begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \end{bmatrix}}_{\mathcal{O}} \underbrace{\left[\underbrace{B \quad AB \quad A^2B \quad \dots}_{\mathcal{C}} \right]}_{x_0} \begin{bmatrix} u_{-1} \\ u_{-2} \\ u_{-3} \\ \vdots \end{bmatrix}$$

Factorization $\mathcal{H} = \mathcal{O}\mathcal{C}$ is not unique, and $\mathcal{H} = (\mathcal{O}T)(T^{-1}\mathcal{C})$ corresponds to the transformed system $\{T^{-1}AT, T^{-1}B, CT\}$

Gramians derived from the Hankel map

Define the dual maps

$$\mathcal{O}^* : y([0, \infty)) \mapsto x(0), \quad \mathcal{C}^* : x(0) \mapsto u((-\infty, 0))$$

and the (observability and controllability) *Gramians*

$$G_o \doteq \mathcal{O}^* \mathcal{O}, \quad G_c \doteq \mathcal{C} \mathcal{C}^*$$

$$G_o = \sum_0^{+\infty} (CA^k)^T (CA^k), \quad G_c = \sum_0^{+\infty} (A^k B)(A^k B)^T,$$

solved by

$$A^T G_o A - G_o + C^T C = 0 \quad \text{and} \quad A G_c A^T - G_c + B B^T = 0.$$

Since $\mathcal{H} = \mathcal{O}\mathcal{C}$ it follows that

$$\mathcal{H}^*\mathcal{H} = \mathcal{C}^*\mathcal{O}^*\mathcal{O}\mathcal{C}, \quad \text{and} \quad G_c G_o \doteq \mathcal{C}\mathcal{C}^*\mathcal{O}^*\mathcal{O}$$

have the same nonzero eigenvalues $\Rightarrow \sigma_i^2(\mathcal{H}) = \lambda_i(G_c G_o)$.

Balancing transformation T

$$\hat{G}_o \doteq T^T G_o T, \quad \hat{G}_c \doteq T^{-1} G_c T^{-T},$$

$$\{\hat{A}, \hat{B}, \hat{C}\} \doteq \{T^{-1}AT, T^{-1}B, CT\} \xleftarrow{T} \{A, B, C\}$$

diagonalizes both Gramians and makes them equal :

$$\hat{\mathcal{O}} = \mathcal{O}T, \quad \hat{\mathcal{C}} = T^{-1}\mathcal{C}, \quad \hat{G}_o = \hat{\mathcal{O}}^*\hat{\mathcal{O}} = \Sigma = \hat{\mathcal{C}}\hat{\mathcal{C}}^* = \hat{G}_c$$

H_∞ and Hankel norms are often close to each other \Rightarrow

New problem : *find the best (stable) approximation $\hat{H}(\cdot)$ of degree n for $H(\cdot)$ in the Hankel norm.*

Approximation via balanced truncation

Partition a balanced system as follows

$$\Sigma \doteq \begin{bmatrix} \Sigma_{11} & 0 \\ 0 & \Sigma_{22} \end{bmatrix}, \quad \sigma_{\min}(\Sigma_{11}) \gg \sigma_{\max}(\Sigma_{22}),$$

and define

$$\hat{A} \doteq \begin{bmatrix} \hat{A}_{11} & \hat{A}_{12} \\ \hat{A}_{21} & \hat{A}_{22} \end{bmatrix}, \hat{B} \doteq \begin{bmatrix} \hat{B}_1 \\ \hat{B}_2 \end{bmatrix}, \hat{C} \doteq \begin{bmatrix} \hat{C}_1 & \hat{C}_2 \end{bmatrix}.$$

Define also

$$\hat{Y}^T \doteq \begin{bmatrix} I_n & 0 \end{bmatrix}, \quad \hat{X} \doteq \begin{bmatrix} I_n \\ 0 \end{bmatrix}, \quad \hat{P} \doteq \hat{X} \hat{Y}^T,$$

Then “truncated” system can be written as

$$\left\{ \hat{A}_{11}, \hat{B}_1, \hat{C}_1 \right\} = \left\{ \hat{Y}^T \hat{A} \hat{X}, \hat{Y}^T \hat{B}, \hat{C} \hat{X} \right\} \quad (1)$$

Since

$$\hat{\mathcal{O}} = \begin{bmatrix} U_1 \Sigma_{11}^{\frac{1}{2}} & U_2 \Sigma_{22}^{\frac{1}{2}} \end{bmatrix}, \quad \hat{\mathcal{C}} = \begin{bmatrix} \Sigma_{11}^{\frac{1}{2}} V_1^T \\ \Sigma_{22}^{\frac{1}{2}} V_2^T \end{bmatrix},$$

then $\hat{\mathcal{O}} \hat{P} \hat{\mathcal{C}} \doteq U_1 \Sigma_{11} V_1^T$ is an “optimal” rank n approximation of \mathcal{H} :

$$\|\mathcal{H} - \hat{\mathcal{O}} \hat{P} \hat{\mathcal{C}}\|_2 = \|\hat{\mathcal{O}} \hat{\mathcal{C}} - \hat{\mathcal{O}} \hat{P} \hat{\mathcal{C}}\|_2 = \|U_2 \Sigma_{22} V_2^T\|_2 = \sigma_{n+1}$$

but it is not Hankel !

If $\sigma_n \gg \sigma_{n+1}$ then (1) has a Hankel map $\hat{\mathcal{H}}$ close to $\hat{\mathcal{O}}\hat{P}\hat{\mathcal{C}}$ and

$$\sigma_{n+1}^2 \leq \|\mathcal{H} - \hat{\mathcal{H}}\|_2^2 \leq \sum_{i=n+1}^N \sigma_i^2$$

Balanced truncation is thus “near optimal” and stable !

In the original system we can also write

$$\{\hat{A}_{11}, \hat{B}_1, \hat{C}_1\} = \{Y^T A X, Y^T B, C X\}$$

where the projector P is given by $P = X Y^T$:

$$Y^T X = I_n, \quad Y^T G_c G_o X = \Sigma^2$$

Also X and Y are “dominant” eigenspaces of $G_c G_o$

Numerical procedure

Solve for the Gramians from

$$A^T G_o A - G_o + C^T C = 0 \quad \text{and} \quad A G_c A^T - G_c + B B^T = 0,$$

then find “dominant spaces” X and Y such that

$$Y^T X = I_n, \quad G_c G_o X = X \Sigma^2, \quad Y^T G_c G_o = \Sigma^2 Y^T$$

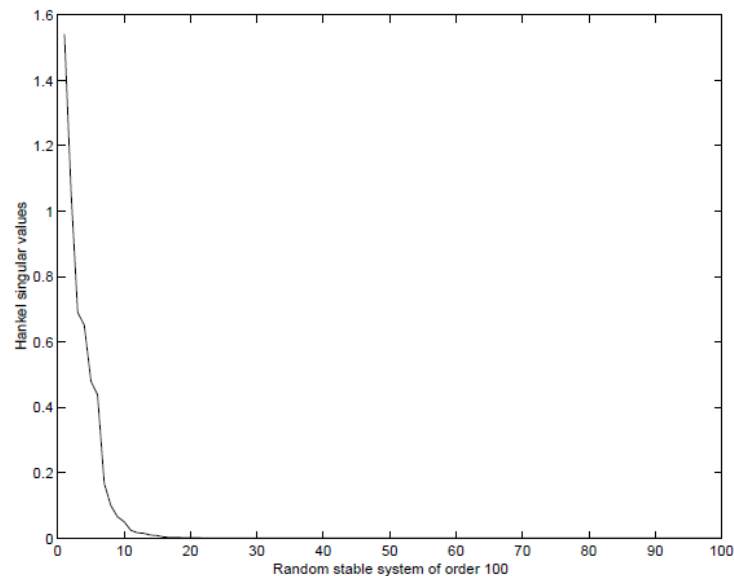
Notice that $U_1 \Sigma_{11}^{\frac{1}{2}} = \mathcal{O} X, \quad Y^T \mathcal{C} = \Sigma_{11}^{\frac{1}{2}} V_1^T$

Problem : behaviour of Hankel singular values

It is known that for $\mathcal{H} > 0$ $\frac{\sigma_1(\mathcal{H})}{\sigma_n(\mathcal{H})} \approx 4^n$!

But for all pass transfer function $\Sigma = I_N$!

Typical behaviour for stable system :



One has to be careful with numerical calculation of Gramians (ill conditioning) and construction of projectors

Square root approach

From

$$G_c = S^T S, \quad G_o = R^T R$$

compute the singular value decomposition

$$SR^T = \left[\begin{array}{c|c} U_1 & U_2 \end{array} \right] \left[\begin{array}{c|c} \Sigma_1 & 0 \\ \hline 0 & \Sigma_2 \end{array} \right] \left[\begin{array}{c|c} V_1 & V_2 \end{array} \right]^T$$

where

$$\Sigma_1 = \text{diag}\{\sigma_1, \dots, \sigma_n\}, \quad \Sigma_2 = \text{diag}\{\sigma_{n+1}, \dots, \sigma_N\},$$

Then define

$$Y = R^T V_1 \Sigma_1^{-\frac{1}{2}}, \quad X = S^T U_1 \Sigma_1^{-\frac{1}{2}},$$

This implies

$$Y^T X = \Sigma_1^{-\frac{1}{2}} V_1^T R S^T U_1 \Sigma_1^{-\frac{1}{2}} = I_n,$$

$$Y^T G_c G_o X = Y^T S^T S R^T R X = \Sigma_1^{\frac{1}{2}} U_1^T S R^T V_1 \Sigma_1^{\frac{1}{2}} = \Sigma_1^2,$$

It follows also that the singular values σ_i of $S R^T$ are the (nonzero) Hankel singular values.

The Gramians $G_c = S^T S$ and $G_o = R^T R$ are not needed to construct the projector $P = Y^T X$, but only the factors S and R !

Other bases for X and Y can be chosen without diagonalizing

$$Y^T G_c G_o X$$

[Varga] computes orthonormal bases via the QR decompositions :

$$S^T U_1 = XW, \quad X^T X = I_n, \quad W \text{ upper triangular}$$

$$R^T V_1 = YZ, \quad Y^T Y = I_n, \quad Z \text{ upper triangular.}$$

Reduced order model is then obtained as

$$\left\{ \hat{A}_{11}, \hat{B}_1, \hat{C}_1 \right\} = \left\{ (Y^T X)^{-1} Y^T A X, (Y^T X)^{-1} Y^T B, C X \right\}$$

Dense Stein solvers (exact)

Bartels-Stewart/Hammarling solver ($O(N^3)$ flops)

1. Compute upper triangular Schur form $A_u \doteq U^T A U$ and put
 $G_u \doteq U^T G_o U$, $C_u \doteq C U$
2. Put $G_u \doteq R^T R$ and solve for columns of R in

$$A_u^T R^T R A_u - R^T R = C_u^T C_u$$

3. Return to original coordinates $G_o = U R^T R U^T$ if needed

Advantages

better conditioned $\kappa(R) = \sqrt{\kappa(G_o)}$

back transformation is not always needed

works for both Gramians in continuous and discrete time

Dense Stein solvers (approximate)

The Stein equation

$$A^T X A + M = X$$

is a special Riccati equation solved via the Disc function.

The corresponding recursive algorithm is the Smith iteration

$$\begin{array}{l} A_0 \leftarrow A, \quad M_0 \leftarrow M, \quad \text{for } k = 0, 1, 2, \dots \\ A_{k+1} \leftarrow A_k^2, \quad M_{k+1} \leftarrow M_k + A_k^T M_k A_k \end{array}$$

Taking the Cholesky factorization $M_k = R_k^T \cdot R_k$ one obtains the next factor R_{k+1} from a QR factorization [Benner et al.] :

$$\begin{bmatrix} R_k \\ R_k A_k \end{bmatrix} \rightarrow Q_{k+1} \cdot R_{k+1}.$$

Interpolation approach (continuous-time)

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases} \quad H(s) = C(sI_N - A)^{-1}B + D$$

$$u_k \in \mathbb{R}^m, y_k \in \mathbb{R}^p, x_k \in \mathbb{R}^N, N \gg m, p$$

Find another system driven with the same input $u_k \in \mathbb{R}^m$

$$\begin{cases} \dot{\hat{x}}(t) = \hat{A}\hat{x}(t) + \hat{B}u(t) \\ \hat{y}(t) = \hat{C}\hat{x}(t) + \hat{D}u(t) \end{cases} \quad \hat{H}(s) = \hat{C}(sI_n - \hat{A})^{-1}\hat{B} + \hat{D}$$

but with different $\hat{y}(t) \in \mathbb{R}^p, \hat{x}(t) \in \mathbb{R}^n$.

Problem : *find the best (stable) approximation $\hat{H}(\cdot)$ of degree n for $H(\cdot)$ in $\|\cdot\|_\infty$ norm.*

Should also approximate Gramians

Interpolating $H(\omega)$ is a good idea because of Parseval's theorem

$$G_o = \frac{1}{2\pi} \int_{-\infty}^{+\infty} (-j\omega I - A^T)^{-1} C^T C (j\omega I - A)^{-1} d\omega,$$

$$G_c = \frac{1}{2\pi} \int_{-\infty}^{+\infty} (j\omega I - A)^{-1} B B^T (-j\omega I - A^T)^{-1} d\omega$$

or fitting the exponential since

$$G_o = \int_0^{+\infty} e^{A^T t} C^T C e^{A t} dt, \quad G_c = \int_0^{+\infty} e^{A t} B B^T e^{A^T t} dt$$

or approximate Lyapunov solvers (ADI)

$$A^T G_o + G_o A = C^T C, \quad A G_c + G_c A^T = B B^T$$

Krylov subspaces

What technique to use ? The discrete-time case :

$$\begin{bmatrix} y_0 \\ y_1 \\ y_2 \\ \vdots \end{bmatrix} = \mathcal{O}C \begin{bmatrix} u_{-1} \\ u_{-2} \\ u_{-3} \\ \vdots \end{bmatrix} = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \end{bmatrix} \begin{bmatrix} B & AB & A^2B & \dots \end{bmatrix} \begin{bmatrix} u_{-1} \\ u_{-2} \\ u_{-3} \\ \vdots \end{bmatrix}$$

... suggests to use Krylov sequences !

$$\mathcal{K}_j(M, R) = \text{Im} \{ R, MR, M^2R, \dots, M^{j-1}R \}$$

Rational interpolation and moment matching

Let X and Y define a projector ($Y^T X = I_n$) and

$$\{\hat{A}, \hat{B}, \hat{C}, D\} = \{Y^T A X, Y^T B, C X, D\}$$

Taylor series of $H(s) \doteq C(sI - A)^{-1}B + D$ around $s = \infty$

$$H(s) = H_0 + H_1 s^{-1} + H_2 s^{-2} + \dots,$$

where the moments H_i are equal to :

$$H_0 = D, \quad H_i = C A^{i-1} B, \quad i = 1, 2, \dots$$

The reduced order model $\hat{H}(s) \doteq \hat{C}(sI - \hat{A})^{-1}\hat{B} + \hat{D}$

Rational interpolation and moment matching

... has a similar expansion

$$\hat{H}(s) = \hat{H}_0 + \hat{H}_1 s^{-1} + \hat{H}_2 s^{-2} + \dots ,$$

with moments \hat{H}_i :

$$\hat{H}_0 = \hat{D}, \quad \hat{H}_i = \hat{C} \hat{A}^{i-1} \hat{B}, \quad i = 1, 2, \dots$$

Theorem : Let $m = p$, $Y^T X = I_n$ and assume

$$\text{Im} X = \text{Im} [B, AB, A^2 B, \dots, A^{k-1} B] ,$$

$$\text{Im} Y = \text{Im} [C^T, A^T C^T, A^{2T} C^T, \dots, A^{(k-1)T} C^T]$$

then the first $2k$ moments match :

$$H_j = \hat{H}_j, \quad j = 1, \dots, 2k.$$

Rational interpolation and moment matching

Lanczos algorithm and Padé approximation

One shows for $p = m = 1$ that $\hat{H}(s)$ is the (Laurent)-Padé approximation to $H(s)$ since the first $2k$ moments are matched.

Is the basis of the Asymptotic Waveform Expansion (AWE) :

- 1) compute the moments H_i
- 2) construct the Padé approximation $\hat{H}(s)$

A more reliable method to construct the reduced order model $\hat{H}(s)$ is to construct directly a realization $\{\hat{A}, \hat{b}, \hat{c}, d\}$ via Lanczos

Rational interpolation and moment matching

Lanczos is numerically better than Padé

Example : stiff RC ladder circuit $C_1 = 10^{-3}$, $C_2 = 10^{-6}$, $C_3 = 10^{-9}$

$$\left[\begin{array}{c|c} A & b \\ \hline c & d \end{array} \right] = \left[\begin{array}{ccc|c} -2C_1^{-1} & C_1^{-1} & 0 & C_1^{-1} \\ C_2^{-1} & -2C_2^{-1} & C_2^{-1} & 0 \\ 0 & C_3^{-1} & -C_3^{-1} & 0 \\ \hline 1 & -1 & 0 & 0 \end{array} \right]$$

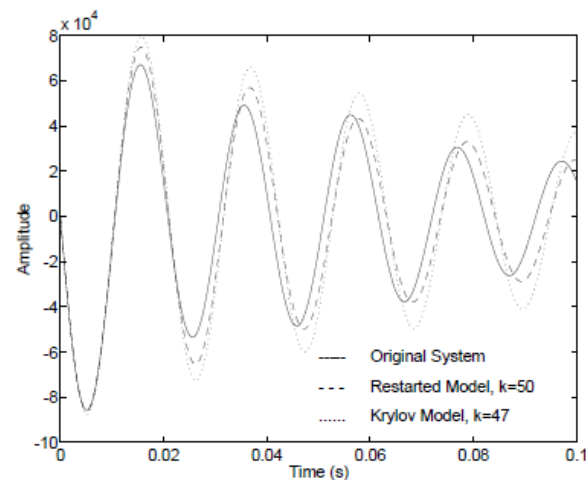
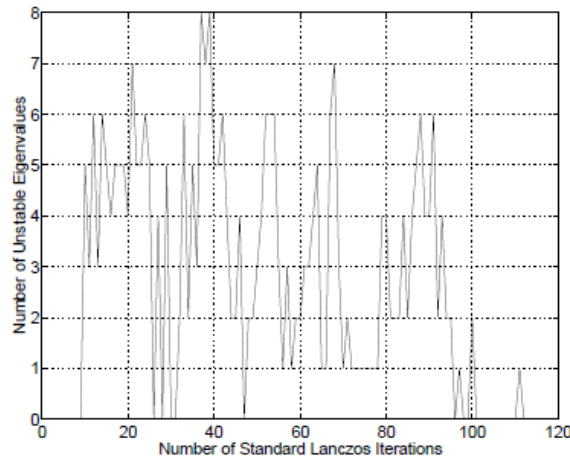
Reconstructed eigenvalues of A from full order model

| | eig 1 | eig 2 | eig 3 |
|--------------|---------------|---------------|---------------|
| Exact | -9.98999000e2 | -1.00000100e6 | -1.00100100e9 |
| Moment Match | -9.98999000e2 | -1.00000078e6 | -5.45486876e6 |
| Lanczos | -9.98999000e2 | -1.00000100e6 | -1.00100100e9 |

Rational interpolation and moment matching

Interpolated models may be unstable !

Unstable eigenvalues of Padé approximants of CD-player



Few model orders are stable (lightly damped system)

Solution (?): Implicitly Restarted Lanczos fits modified moments

$$C\phi(A)A^{i-1}B = \hat{C}\phi(\hat{A})\hat{A}^{i-1}\hat{B}, \quad i = 1, \dots, 2k$$

Rational interpolation and moment matching

Extension to other bases

Any basis X, Y for the same (Krylov) spaces yields the **same** transfer function $\hat{H}(s)$ provided the reduced model is defined as

$$\{\hat{A}, \hat{B}, \hat{C}, D\} = \{(Y^T X)^{-1} Y^T A X, (Y^T X)^{-1} Y^T B, C X, D\}$$

Use two Arnoldi processes instead of one unsymmetric Lanczos

Block Arnoldi process

An orthogonal basis V for the (block) Krylov subspace

$$\mathcal{K}_\ell(A, B) = \text{Im} \{B, AB, A^2 B, \dots, A^{\ell-1} B\}$$

Better numerical properties but slower

Rational interpolation and moment matching

Need for multi-point approximations

We can move the approximation problem to another point

$$H(s) = H_0 + H_1(s - \sigma)^1 + H_2(s - \sigma)^2 + \cdots,$$

where the **moments** H_i are equal to :

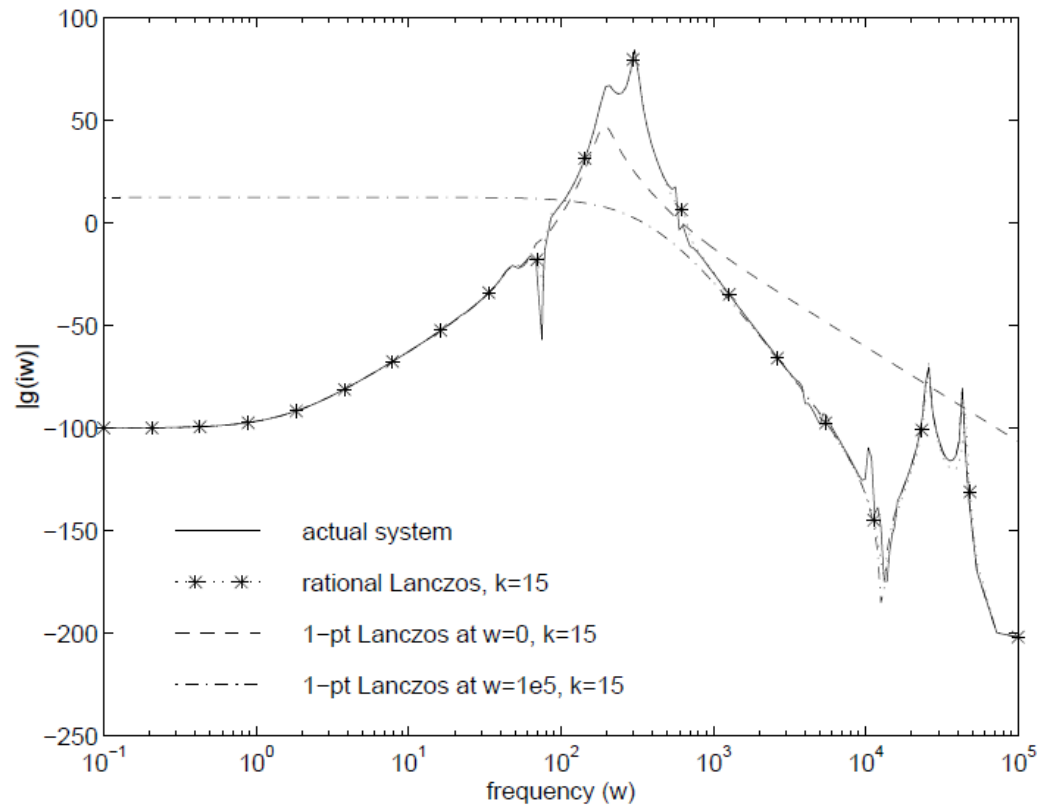
$$H_0 \doteq H(\sigma) = D - C(A - \sigma I)^{-1}B,$$

$$H_i \doteq \frac{1}{i!} \frac{\partial^i H(s)}{\partial s^i} \bigg|_{s=\sigma} = -C(A - \sigma I)^{-(i+1)}B, \quad i > 0.$$

Interpolate $H(s)$ and its derivatives at σ can be transformed to the first problem.

Rational interpolation and moment matching

Yet



indicates that multi-point approximations are better

| |
|-------------------------------|
| General theorem (state-space) |
|-------------------------------|

Consider multiple points $\{\sigma^{(1)}, \dots, \sigma^{(K)}\}$ and the moments

$$H_i^{(k)} = -C(A - \sigma^{(k)}I)^{-(i-1)}B,$$

of the original model, and

$$\hat{H}_i^{(k)} = -\hat{C}(\hat{A} - \sigma^{(k)}I)^{-(i-1)}\hat{B}.$$

of the reduced order model.

Moment matching at the interpolation points $\sigma^{(k)}, k = 1, \dots, K$ is completely described by the following theorem :

(Notice that **inclusion** is sufficient !)

Theorem : If

$$\bigcup_{k=1}^K \mathcal{K}_{J_{b_k}} \left((A - \sigma^{(k)} I)^{-1}, (A - \sigma^{(k)} I)^{-1} B \right) \subseteq \text{Im} X$$

and

$$\bigcup_{k=1}^K \mathcal{K}_{J_{c_k}} \left((A - \sigma^{(k)} I)^{-T}, (A - \sigma^{(k)} I)^{-T} C^T \right) \subseteq \text{Im} Y$$

then the moments $H_i^{(k)}$ of the system $\{A, B, C, D\}$ and the corresponding moments $\hat{H}_i^{(k)}$ of the reduced order model

$$\{(Y^T X)^{-1} Y^T A X, (Y^T X)^{-1} Y^T B, C X, D\}$$

match up to $J_{(k)} \doteq J_{b_k} + J_{c_k}$:

$$H_i^{(j_k)} = \hat{H}_i^{(j_k)}, \quad j_k = 1, 2, \dots, J_{(k)}, \quad k = 1, 2, \dots, K$$

provided $Y^T X$ is invertible.

Implicit continuous LTI systems

$$\begin{cases} E\dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) \end{cases} \quad H(s) = C(sE - A)^{-1}B$$

$$u_k \in \mathbb{R}^m, y_k \in \mathbb{R}^p, x_k \in \mathbb{R}^N, N \gg m, p$$

Find another system driven with the same input $u_k \in \mathbb{R}^m$

$$\begin{cases} \hat{E}\dot{\hat{x}}(t) = \hat{A}\hat{x}(t) + \hat{B}u(t) \\ \hat{y}(t) = \hat{C}\hat{x}(t) \end{cases} \quad \hat{H}(s) = \hat{C}(s\hat{E} - \hat{A})^{-1}\hat{B}$$

but with different $\hat{y}(t) \in \mathbb{R}^p, \hat{x}(t) \in \mathbb{R}^n$.

The n th order model is defined from $X, Y \in \mathbb{R}^{N \times n}$:

$$\{\hat{E}, \hat{A}, \hat{B}, \hat{C}\} \doteq \{Y^T EX, Y^T AX, Y^T B, CX\}.$$

The transfer function moments

$$\left. \frac{\partial^i H(s)}{\partial s^i} \right|_{s=\sigma} \doteq i! H_i ,$$

yield an expansion around each interpolation point σ

$$H_i = -C(A - \sigma E)^{-1} \{E(A - \sigma E)^{-1}\}^i B,$$

$$H_i = -C\{(A - \sigma E)^{-1}E\}^i (A - \sigma E)^{-1} B,$$

on which we will base the Krylov spaces

$$\mathcal{K}_j(M, G) = \text{Im} \{G, MG, M^2G, \dots, M^{j-1}G\}$$

Generalized moment condition :

Theorem : If

$$\bigcup_{k=1}^K \mathcal{K}_{J_{b_k}} \left((A - \sigma^{(k)} E)^{-1} E, (A - \sigma^{(k)} E)^{-1} B \right) \subseteq \text{Im} X$$

and

$$\bigcup_{k=1}^K \mathcal{K}_{J_{c_k}} \left((A - \sigma^{(k)} E)^{-T} E^T, (A - \sigma^{(k)} E)^{-T} C^T \right) \subseteq \text{Im} Y$$

then the moments $H_i^{(k)}$ of the system $\{E, A, B, C\}$ and the corresponding moments $\hat{H}_i^{(k)}$ of the reduced order model

$$\{Y^T E X, Y^T A X, Y^T B, C X\}$$

match up to $J_{(k)} \doteq J_{b_k} + J_{c_k}$:

$$H_i^{(j_k)} = \hat{H}_i^{(j_k)}, \quad j_k = 1, 2, \dots, J_{(k)}, \quad k = 1, 2, \dots, K$$

provided the pencil $sY^T E X - Y^T A X$ is regular.

This includes modal matching

Theorem Let $\text{Im}X_i, \text{Im}Y_i$ be left and right invariant subspaces of the regular pencil $(\lambda E - A)$ with given spectrum, then the reduced order pencil $(\lambda \hat{E} - \hat{A}) \doteq Y^T(\lambda E - A)V$ has a right invariant subspace with the same spectrum if

$$\text{Im}X_i \subseteq \text{Im}X$$

and has a left invariant subspace with the same spectrum if

$$\text{Im}Y_i \subseteq \text{Im}Y.$$

This extension allows to incorporate matching poles of the original system into the reduced order system.

Importance :

Approximation of DAE requires often that the reduced order system has the same algebraic conditions (these corresponds to an invariant subspace at ∞)

Tangential interpolation

Consider the MIMO error function $E(s) := H(s) - \hat{H}(s)$

Standard interpolation at $s = \sigma$ implies $E(\sigma) = 0$

Tangential interpolation conditions at $s = \sigma$ are less restrictive :

$$E(\sigma)v(\sigma) = 0, \quad w(\sigma)E(\sigma) = 0, \quad w(\sigma)E(\sigma)v(\sigma),$$

where $w(s)$ and $v(s)$ are (polynomial) row and column vectors

There also exist higher order conditions :

$$E(s)v(s) = 0(s - \sigma)^k, \quad w(s)E(s) = 0(s - \sigma)^k, \quad w(s)E(s)v(s) = 0(s - \sigma)^k$$

which are obtained via generalized Krylov methods or via Sylvester equations

Tangential interpolation

The interpolation condition

$$\left[C(sI_N - A)^{-1}B - \hat{C}(sI_n - \hat{A})^{-1}\hat{B} \right] v(s) = O(s - \sigma)^k$$

is obtained via the generalized Krylov space inclusion

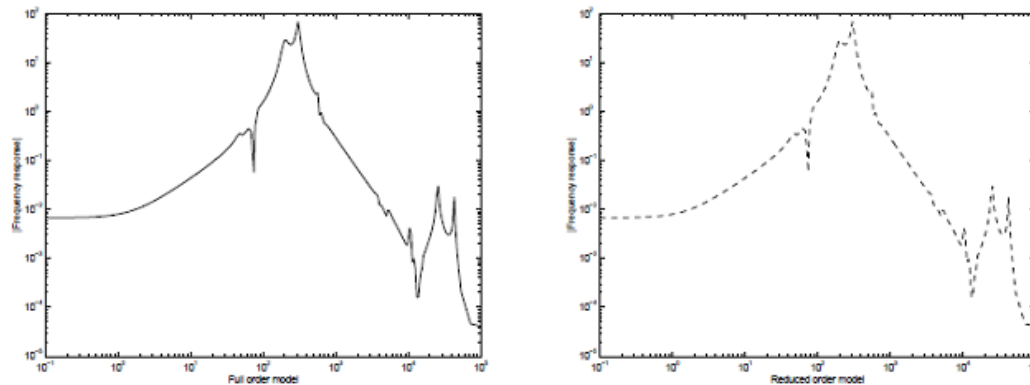
$$\left[(\sigma I_N - A)^{-1}B \dots (\sigma I_N - A)^{-k}B \right] \begin{bmatrix} v_0 & \dots & v_{k-1} \\ & \ddots & \vdots \\ & & v_0 \end{bmatrix} \subseteq \text{Im}(X)$$

or by solving the Sylvester equation $AX - X\tilde{A} = B\tilde{B}$ with

$$\tilde{A} = \sigma I_k - \begin{bmatrix} 0 & 1 & & \\ & \ddots & \ddots & \\ & & 0 & 1 \\ & & & 0 \end{bmatrix}, \tilde{B} = \begin{bmatrix} v_0 & \dots & v_{k-1} \end{bmatrix}$$

H_2 optimal approximations

Minimizing the cost $\mathcal{J} := \|E(z)\|_{\mathcal{H}_2} := \text{tr} \int_{-\infty}^{\infty} E(e^{j\omega}) E(e^{j\omega})^H \frac{d\omega}{2\pi}$ ensures the frequency response to match



and the time responses to match if $H(z)$ and $\hat{H}(z)$ are stable since

$$\mathcal{J} = \text{tr} \sum_{k=0}^{\infty} (C_e A_e^k B_e) (C_e A_e^k B_e)^T$$

with

$$(A_e, B_e, C_e) := \left(\begin{bmatrix} A & \\ & \hat{A} \end{bmatrix}, \begin{bmatrix} B \\ \hat{B} \end{bmatrix}, [C \quad -\hat{C}] \right),$$

How evaluate this norm ?

$$\mathcal{J} = \text{tr} (C_e P_e C_e^T) = \text{tr} (B_e^T Q_e B_e)$$

where P_e and Q_e solve the Stein equations

$$A_e P_e A_e^T + B_e B_e^T = P_e, \quad A_e^T Q_e A_e + C_e^T C_e = Q_e$$

One can also partition

$$P_e := \begin{bmatrix} P & X \\ X^T & \hat{P} \end{bmatrix}, \quad Q_e := \begin{bmatrix} Q & Y \\ Y^T & \hat{Q} \end{bmatrix}$$

and solve

$$\begin{bmatrix} A & \\ & \hat{A} \end{bmatrix} \begin{bmatrix} P & X \\ X^T & \hat{P} \end{bmatrix} \begin{bmatrix} A^T & \\ & \hat{A}^T \end{bmatrix} + \begin{bmatrix} B \\ \hat{B} \end{bmatrix} \begin{bmatrix} B^T & \hat{B}^T \end{bmatrix} = \begin{bmatrix} P & X \\ X^T & \hat{P} \end{bmatrix},$$
$$\begin{bmatrix} A^T & \\ & \hat{A}^T \end{bmatrix} \begin{bmatrix} Q & Y \\ Y^T & \hat{Q} \end{bmatrix} \begin{bmatrix} A & \\ & \hat{A} \end{bmatrix} + \begin{bmatrix} C^T \\ -\hat{C}^T \end{bmatrix} \begin{bmatrix} C & -\hat{C} \end{bmatrix} = \begin{bmatrix} Q & Y \\ Y^T & \hat{Q} \end{bmatrix}$$

Gradients are easier

Let us define the gradient of a scalar function $f(X)$ as

$$[\nabla_X f(X)]_{i,j} = \frac{d}{dX_{i,j}} f(X), \quad i = 1, \dots, n, \quad j = 1, \dots, p$$

then the gradients $\nabla_{\hat{A}} \mathcal{J}, \nabla_{\hat{B}} \mathcal{J}, \nabla_{\hat{C}} \mathcal{J}$ satisfy the equations

$$\frac{1}{2} \nabla_{\hat{A}} \mathcal{J} = \hat{Q} \hat{A} \hat{P} + Y^T A X, \quad \frac{1}{2} \nabla_{\hat{B}} \mathcal{J} = \hat{Q} \hat{B} + Y^T B, \quad \frac{1}{2} \nabla_{\hat{C}} \mathcal{J} = \hat{C} \hat{P} - C X$$

where

$$\begin{aligned} A^T Y \hat{A} - C^T \hat{C} &= Y, \quad \hat{A}^T \hat{Q} \hat{A} + \hat{C}^T \hat{C} = \hat{Q}, \\ \hat{A} X^T A^T + \hat{B} B^T &= X^T, \quad \hat{A} \hat{P} \hat{A}^T + \hat{B} \hat{B}^T = \hat{P} \end{aligned}$$

This is quite cheap to solve (sparse matrix techniques)!

This result is due to Wilson (1970) and was «revisited» by several others (Hyland Bernstein, Halevi, Gugercin-Antoulas-Beattie, VD-Gallivan-Absil, Bunse-Gerstner-Kubalinska-Vossen-Wilczek)

Leads to a fixed point iteration

Define $(X, Y, \hat{P}, \hat{Q}) = F(\hat{A}, \hat{B}, \hat{C})$ where

$$A^T Y \hat{A} - C^T \hat{C} = Y, \quad \hat{A}^T \hat{Q} \hat{A} + \hat{C}^T \hat{C} = \hat{Q},$$

$$\hat{A} X^T A^T + \hat{B} \hat{B}^T = X^T, \quad \hat{A} \hat{P} \hat{A}^T + \hat{B} \hat{B}^T = \hat{P}$$

and then compute $(\hat{A}, \hat{B}, \hat{C}) = G(X, Y, \hat{P}, \hat{Q})$ from

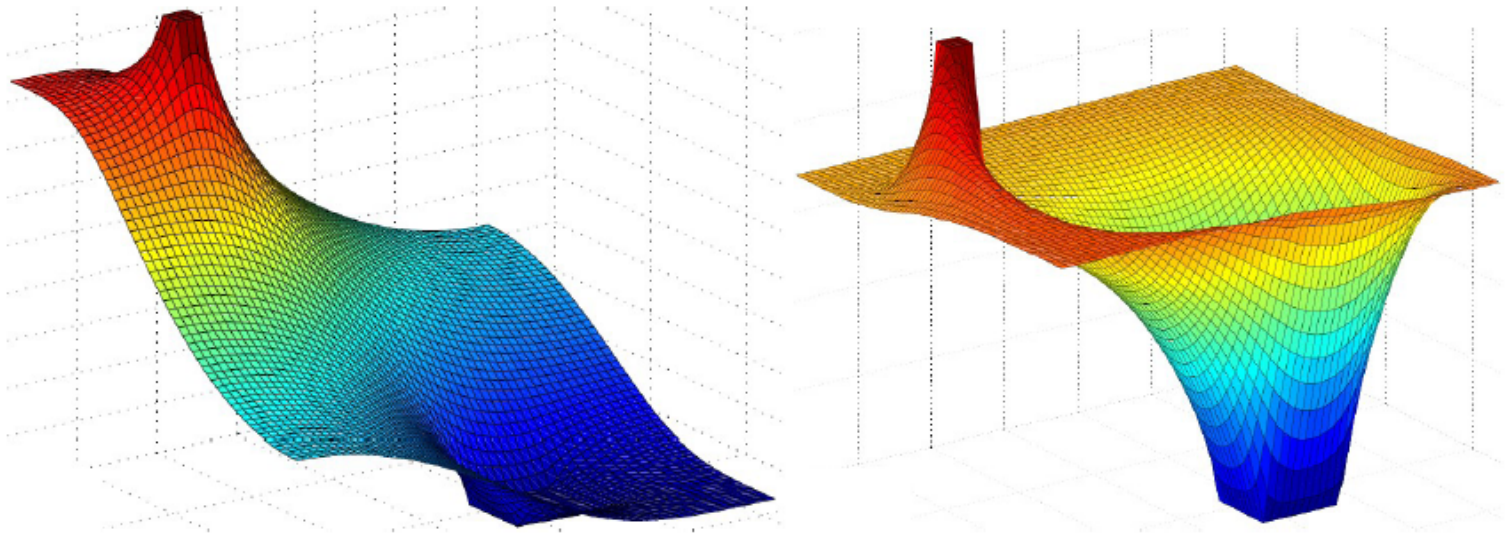
$$W := -Y \hat{Q}^{-1}, \quad V := X \hat{P}^{-1} \quad \hat{A} = W^T A V, \quad \hat{B} = W^T B, \quad \hat{C} = C V,$$

The fixed point of $(\hat{A}, \hat{B}, \hat{C}) = G(F(\hat{A}, \hat{B}, \hat{C}))$ are also stationary points of $\|E(z)\|_{\mathcal{H}_2}$

The basic idea is in essence due to Sorensen-Antoulas and made more formal in Gugercin-Antoulas-Beattie (IRKA)

A PDE example on a FE mesh

Approximating the dynamic of boundary value problem



Examples : diffusion and convection/diffusion equation

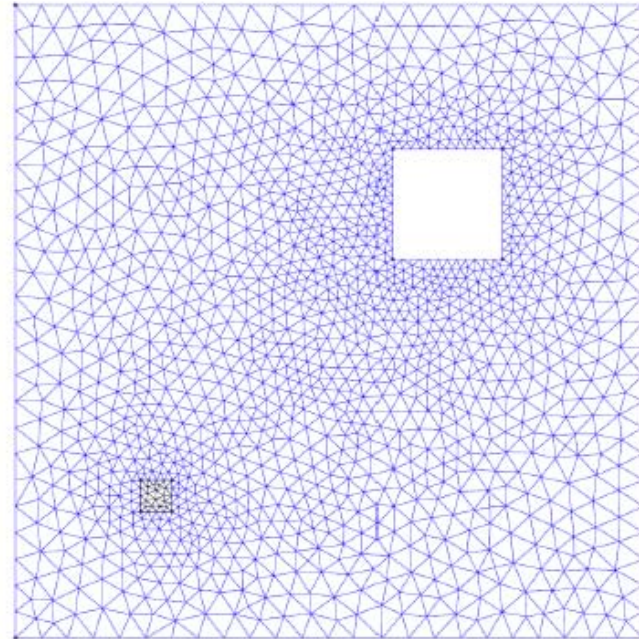
We will assume

Finite element grids
are cheap to generate
for every resolution

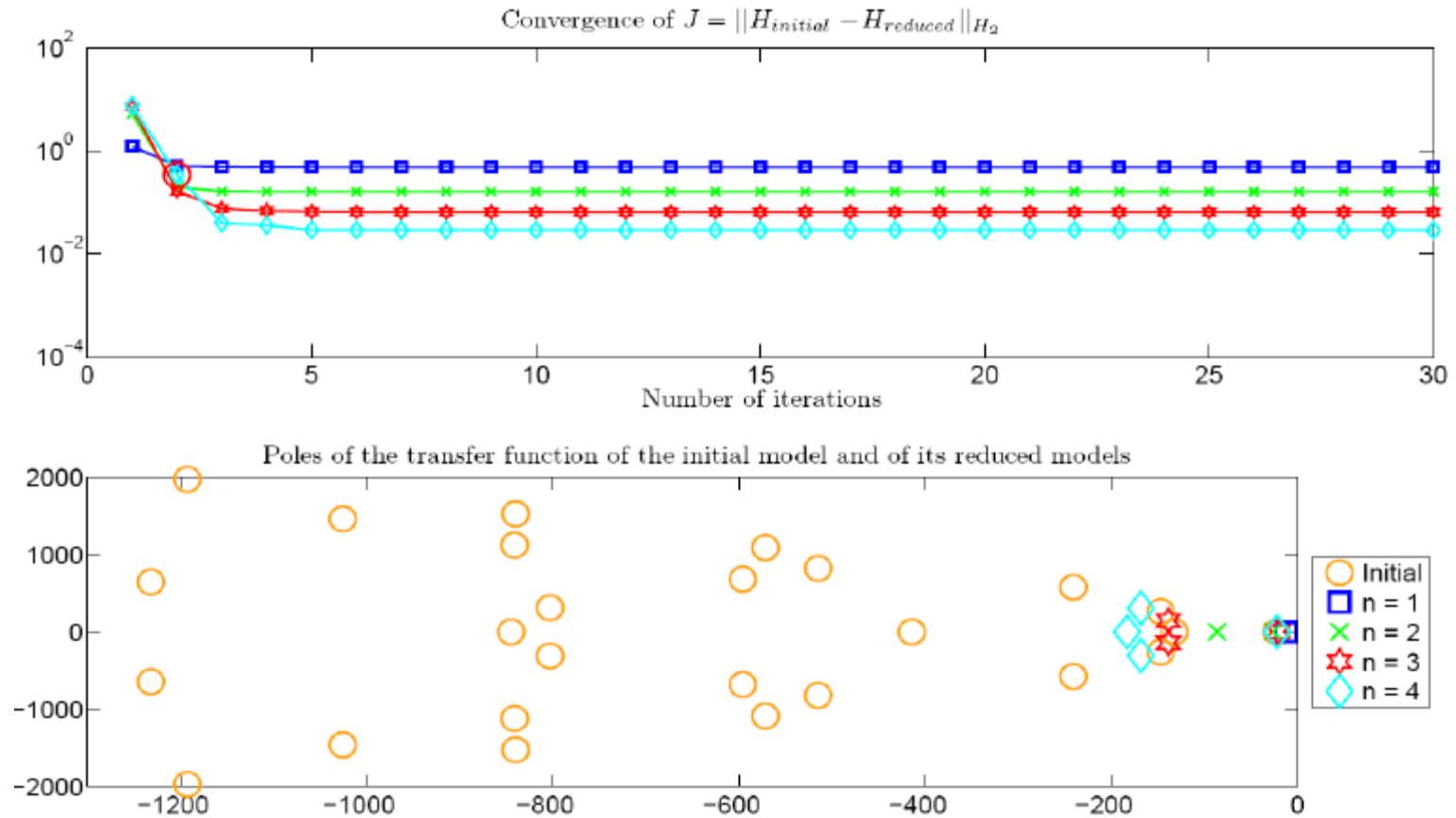
The models are

- Linear time-invariant or
- Linear time-varying

H_2 approximations give good results

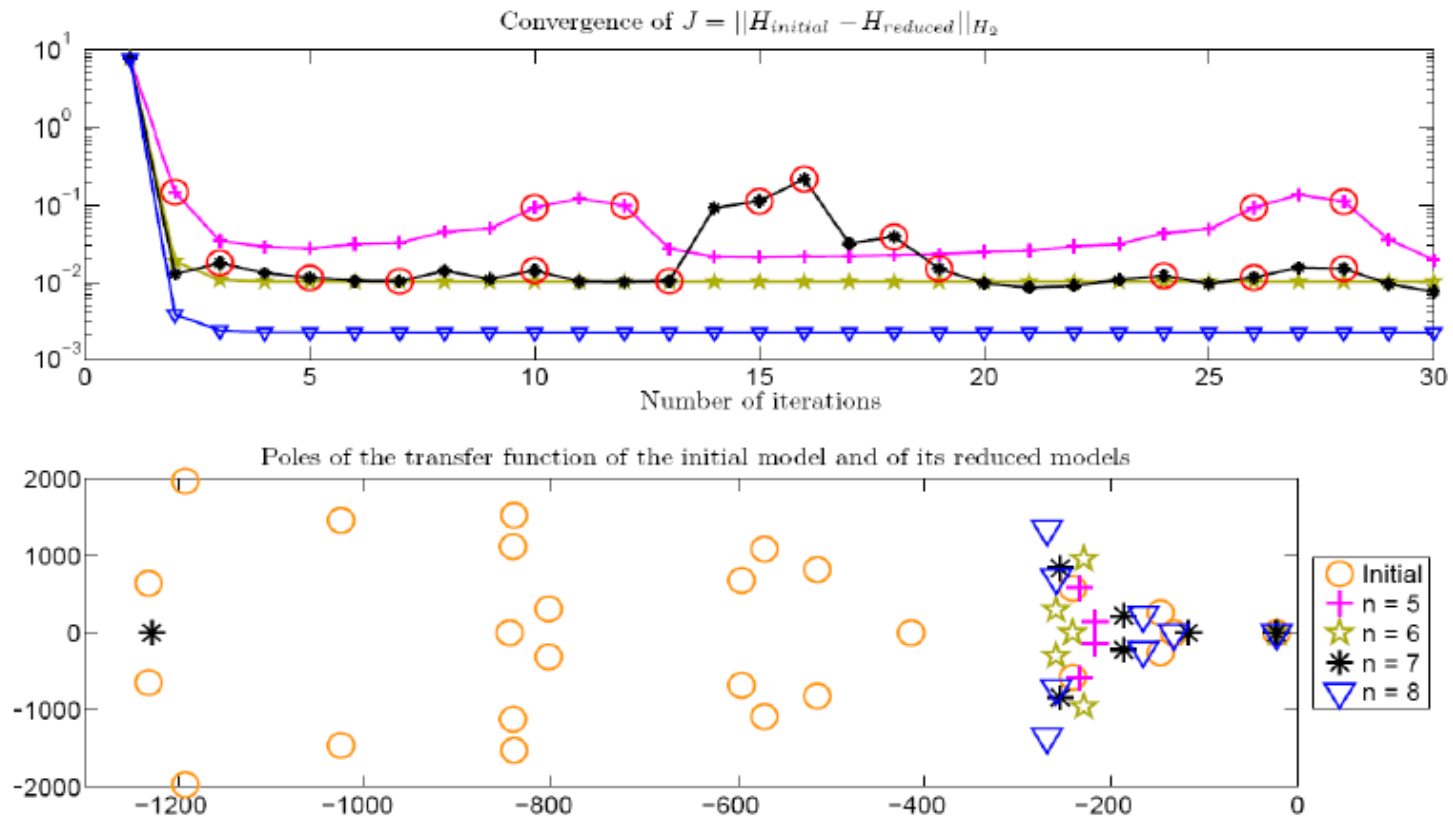


Fixed point iteration often converges ...

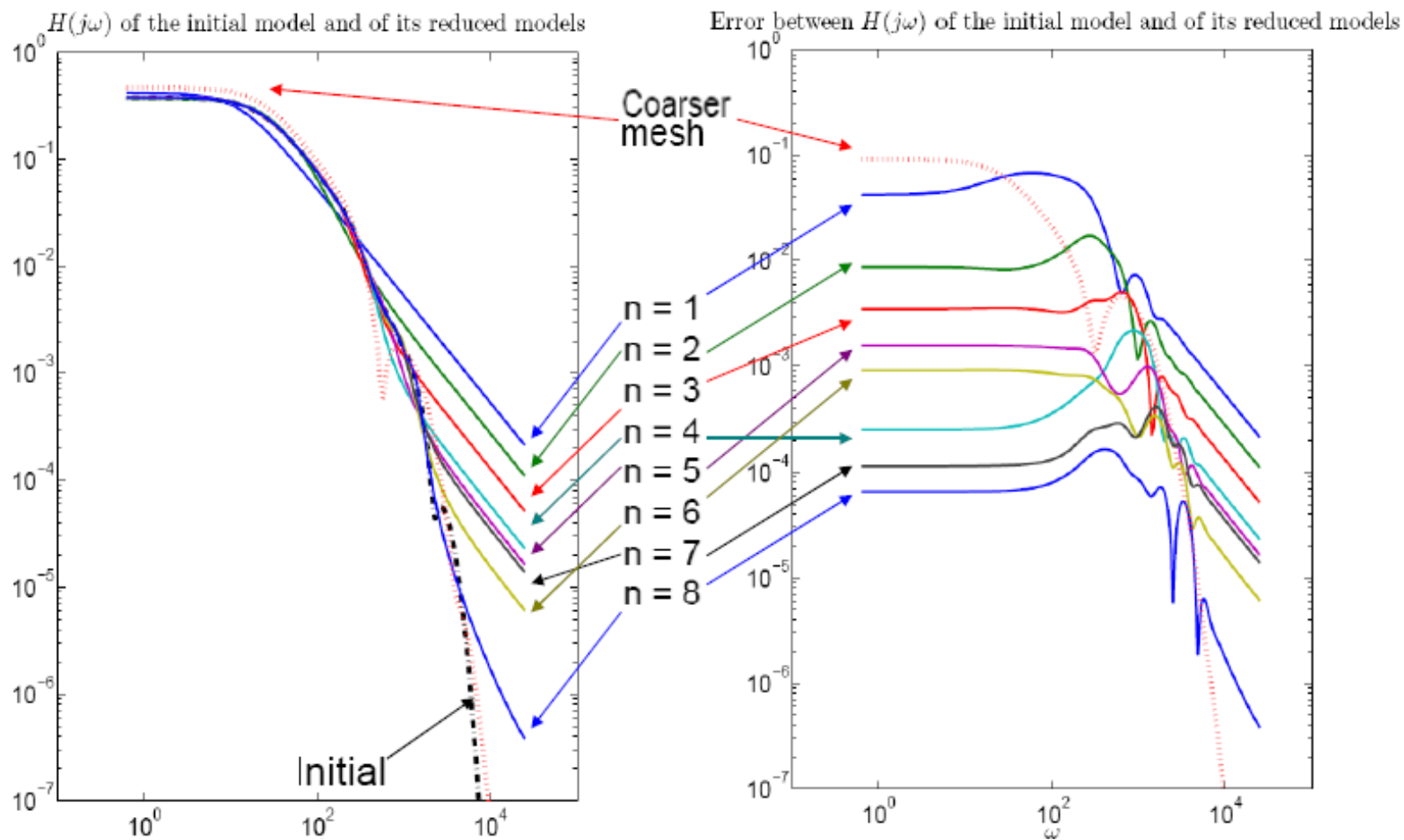


but can also be erratic

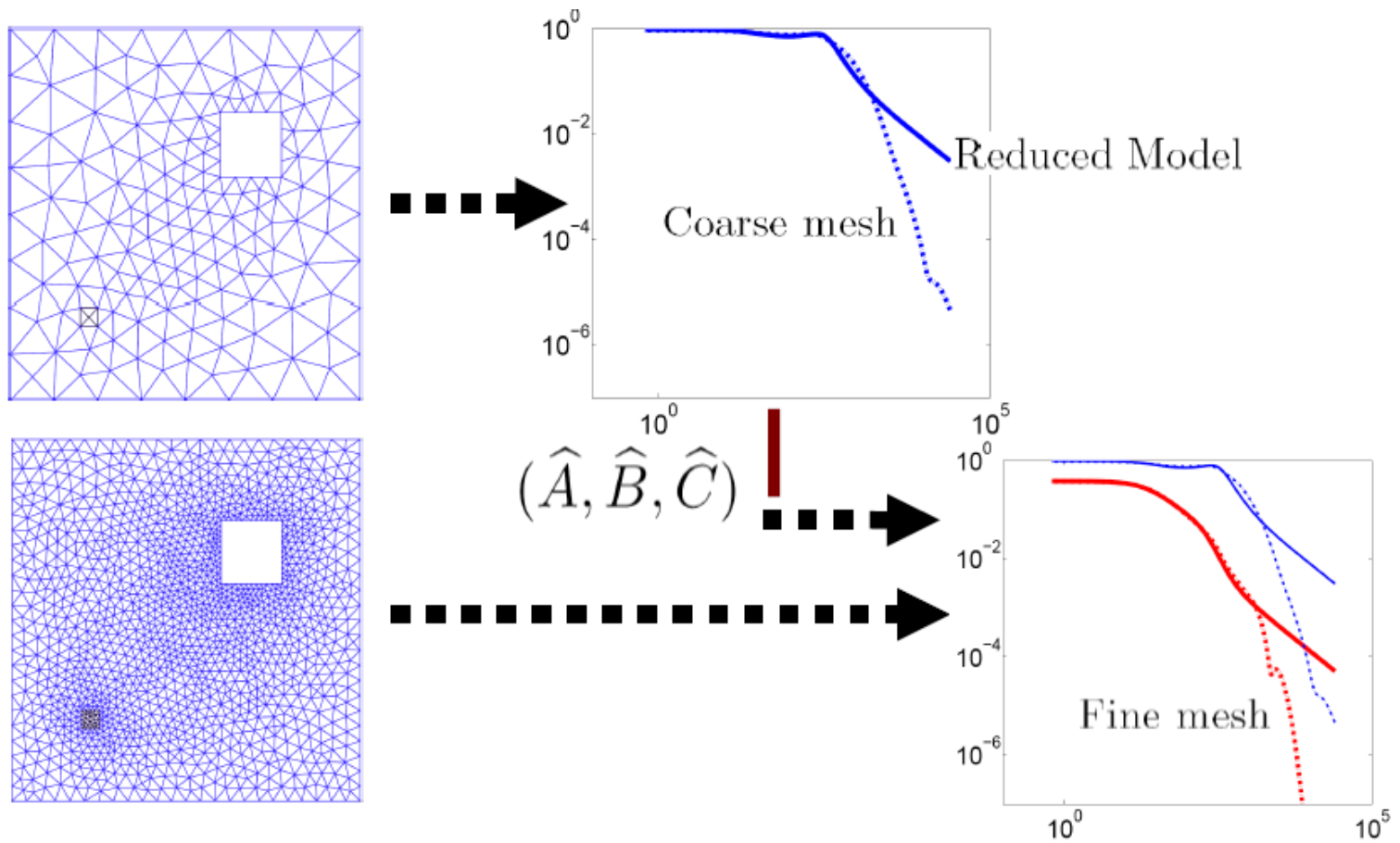
Because intermediate steps can yield unstable systems



Approximation errors

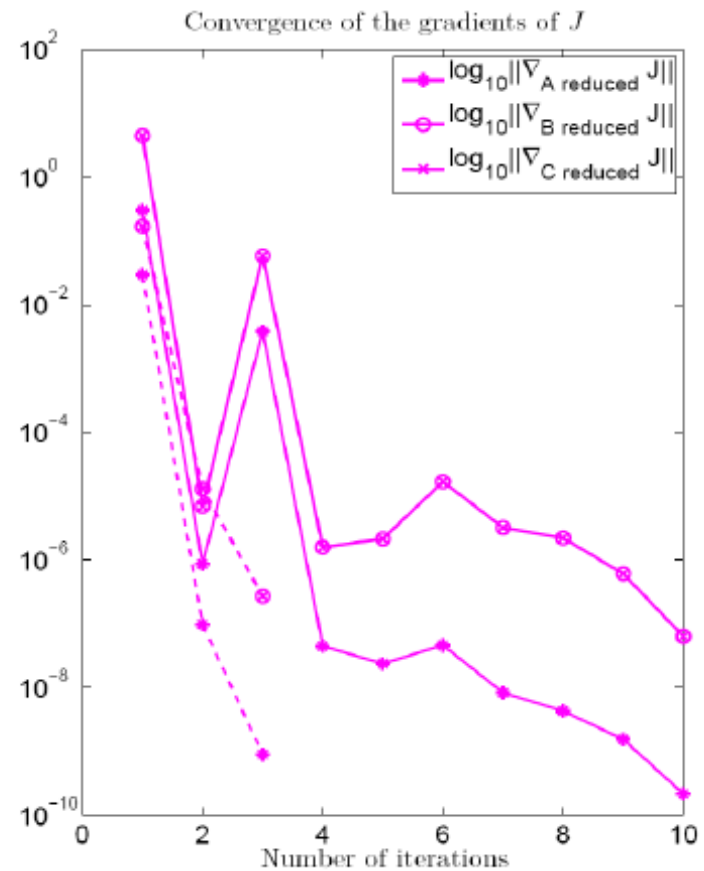
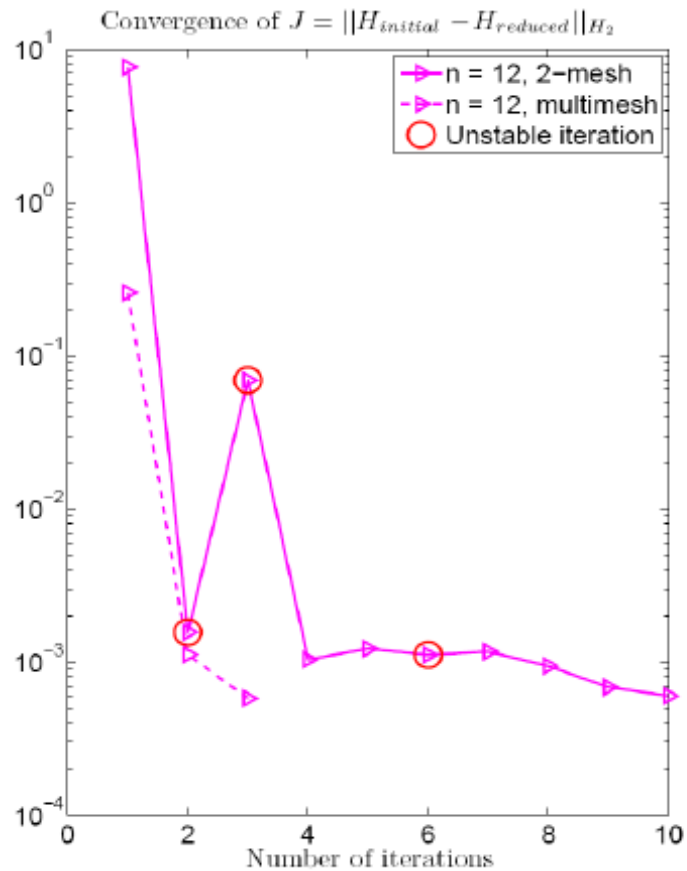


Multilevel idea



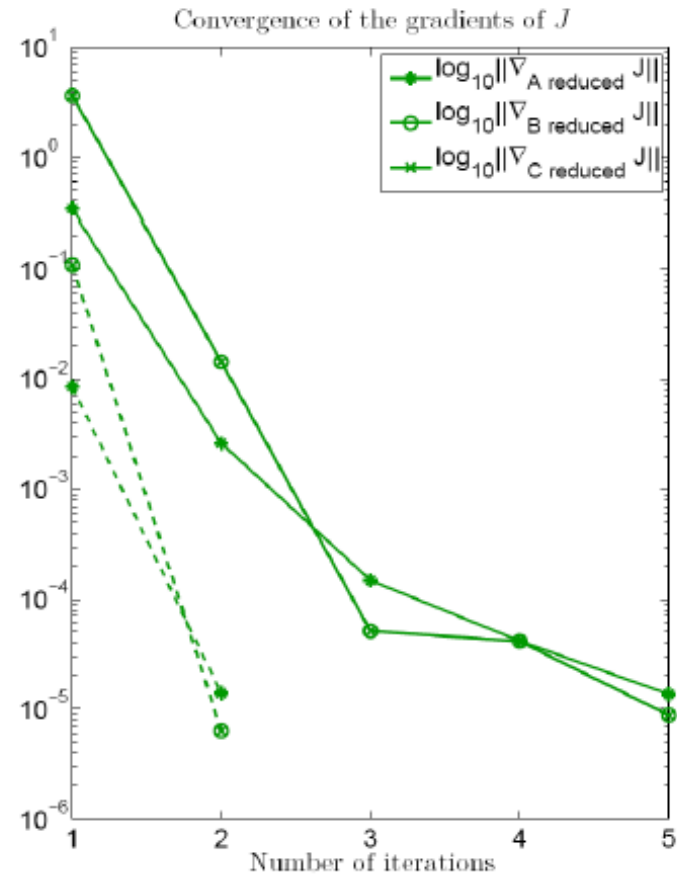
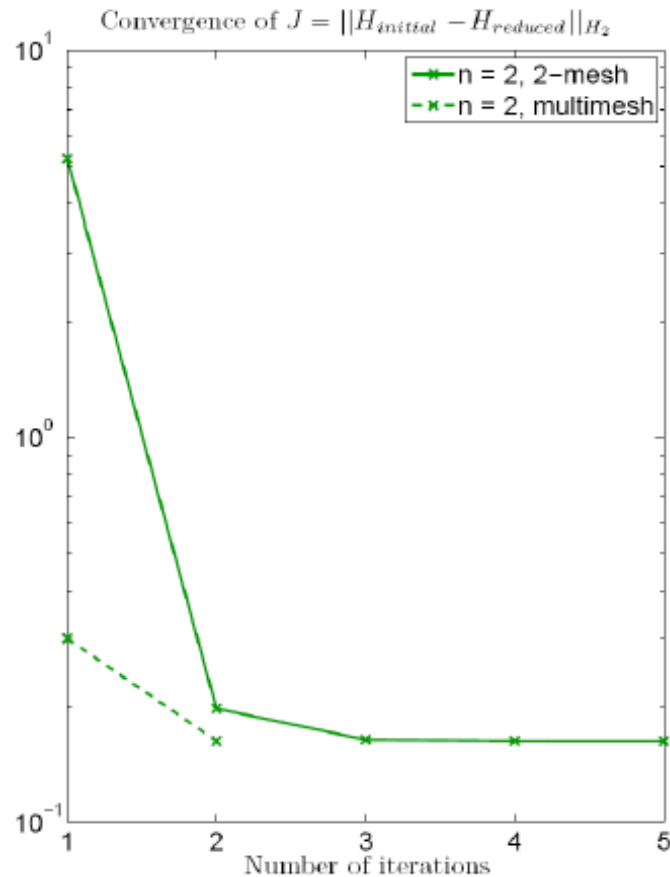
Experiments

Unstable intermediate systems are now avoided



Experiments

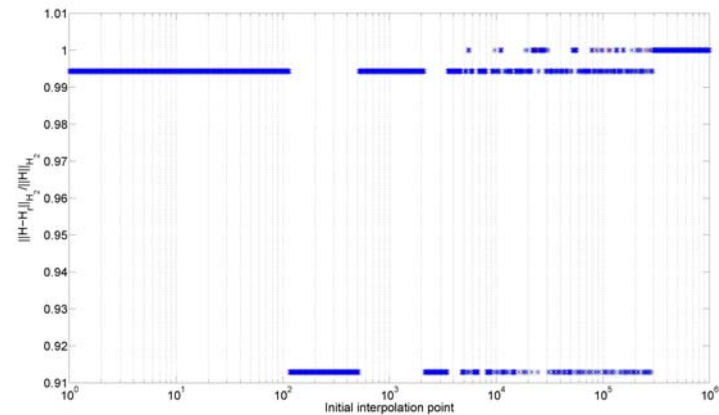
Multilevel method requires only one or two (final) steps



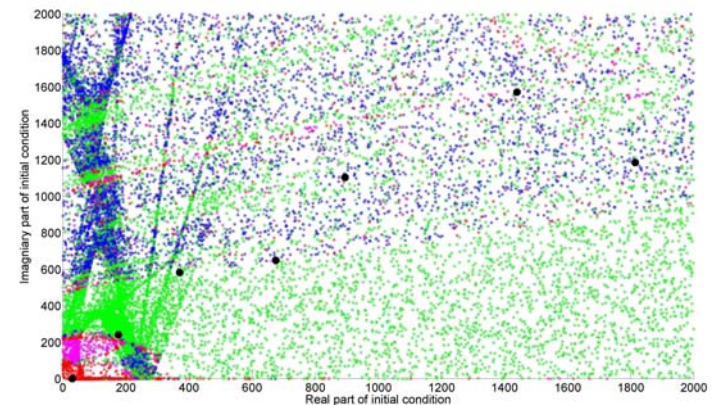
Convergence is delicate

Basins of attraction of different local minima of low order error function

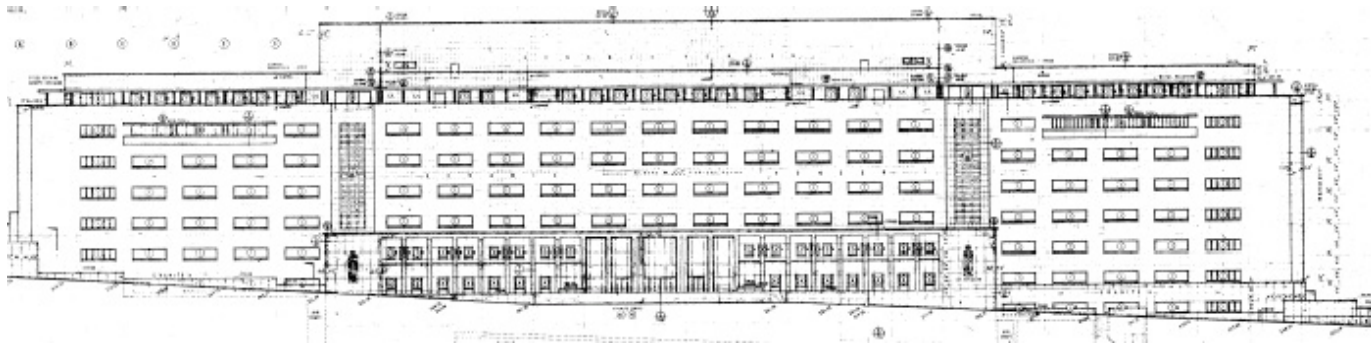
Order 1 approximation
Approximation error vs
Initial interpolation point



Order 2 approximation
Basin of attraction vs
Initial interpolation points



A mechanical application



Modeling of mechanical structures

Identification/calibration (cheap sensors)

Simulation/validation (prognosis)

Model reduction

Control (earthquakes, large flexible structures)

Passive / Semi-Active Fluid Dampers



Passive fluid dampers contain bearings and oil absorbing seismic energy. Semi-active dampers work with variable orifice damping.

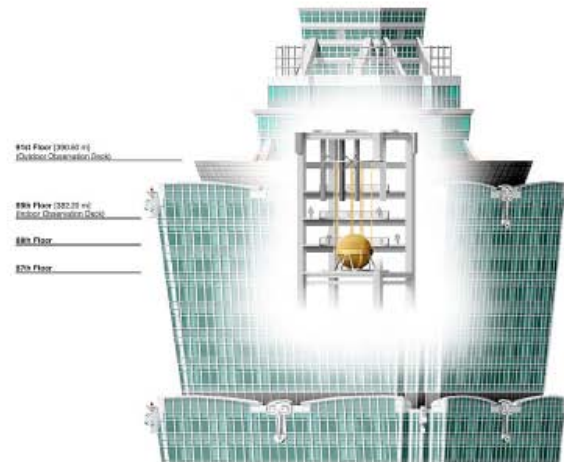
(Picture courtesy Steven Williams)

More examples of Control Mechanisms

Taipei 101: 508m



Damper between 87-91 floors

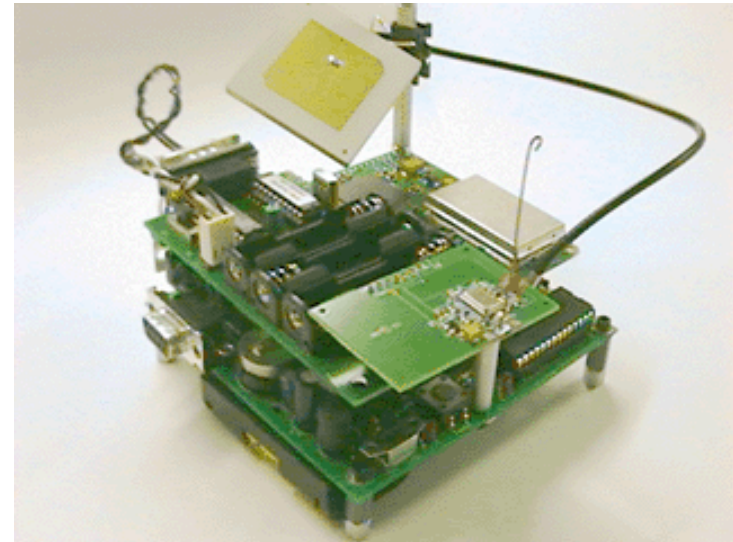
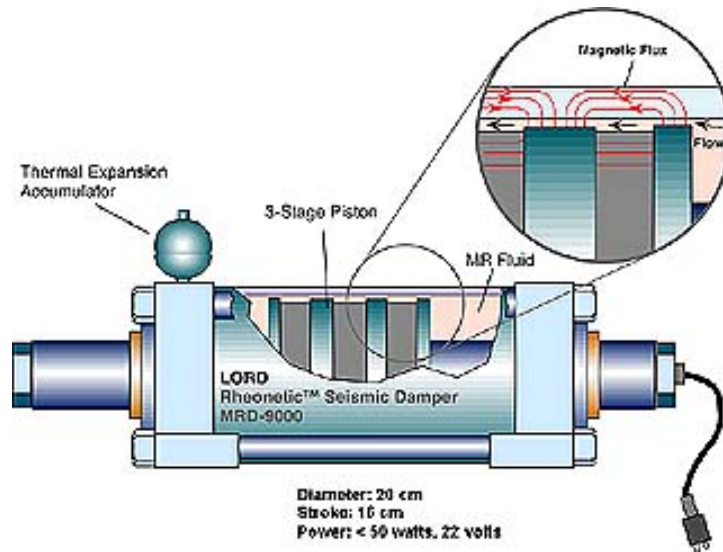


730 ton damper



| Building | Height | Control mechanism | Damping frequency Damping mass |
|--------------------------|--------|-------------------------------|-----------------------------------|
| CN Tower, Toronto | 533 m | Passive tuned mass damper | |
| Hancock building, Boston | 244 m | Two passive tuned dampers | 0.14Hz, 2x300t |
| Sydney tower | 305 m | Passive tuned pendulum | 0.1, 0.5z, 220t |
| Rokko Island P&G, Kobe | 117 m | Passive tuned pendulum | 0.33-0.62Hz, 270t |
| Yokohama Landmark tower | 296 m | Active tuned mass dampers (2) | 0.185Hz, 340t |
| Shinjuku Park Tower | 296 m | Active tuned mass dampers (3) | 330t |
| TYG Building, Atsugi | 159 m | Tuned liquid dampers (720) | 0.53Hz, 18.2t |

The Future: Fine-Grained Semi-Active Control



Dampers are based on Magneto-Rheological fluids with viscosity that changes in milliseconds, when exposed to a magnetic field.

New sensing and networking technology allows to do fine-grained real-time control of structures subjected to winds, earthquakes or hazards.

(Pictures courtesy Lord Corp.)

This technology starts to be applied...



Dongting Lake Bridge has now MR dampers to control wind-induced vibration
(Pictures courtesy of Prof. Y. L. Xu, Hong Kong Poly.)

Second order system models

Model derived from finite element discretization yield systems of the type

$$M\ddot{x}(t) + D\dot{x}(t) + Sx(t) = Bu(t), \quad y(t) = Cx(t)$$

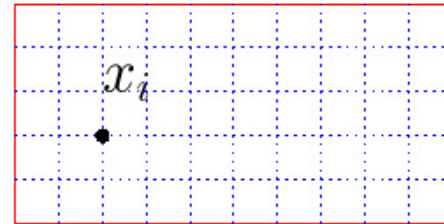
whose solutions describe “vibrations” in the structure

where

M is the mass matrix ($M = M^T \succ 0$)

S is the stiffness matrix ($S = S^T \succ 0$)

$D(\omega)$ is the damping matrix (frequency dependent)



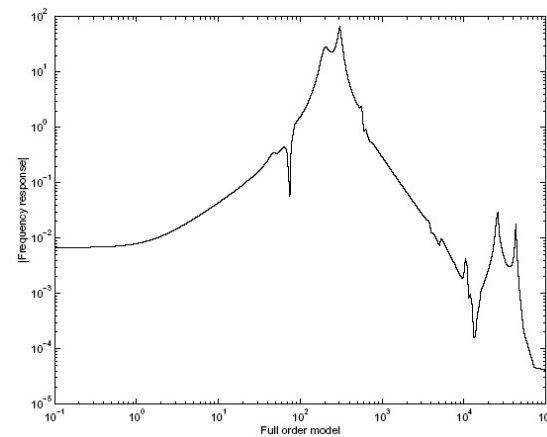
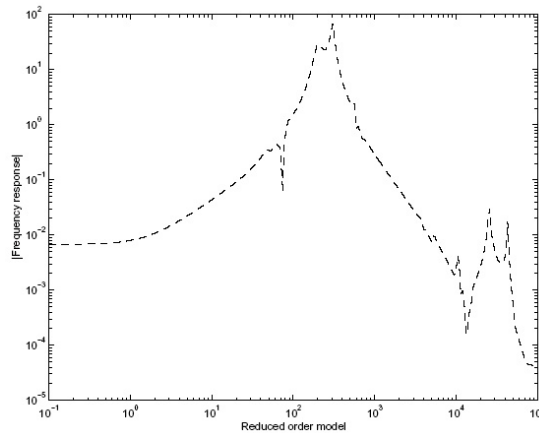
Reduced order model

look for smaller model

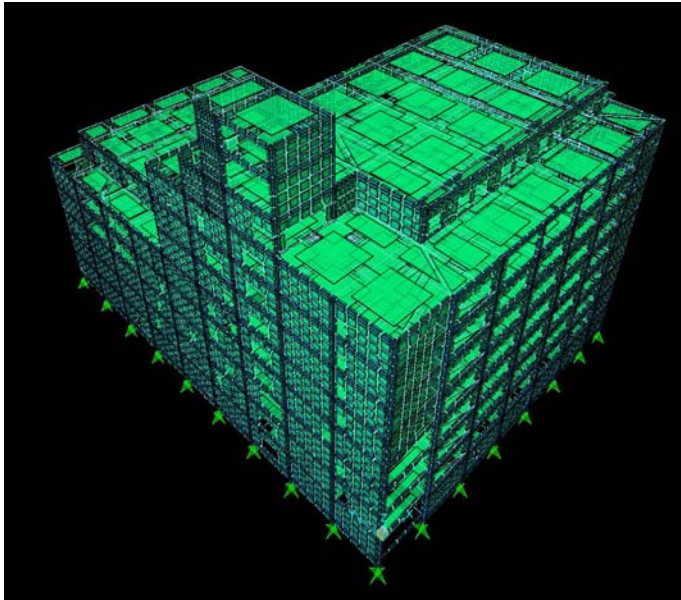
$$\hat{M}\ddot{\hat{x}}(t) + \hat{D}\dot{\hat{x}}(t) + \hat{S}\hat{x}(t) = \hat{B}u(t), \quad \hat{y}(t) = \hat{C}\hat{x}(t)$$

where $u(t) \in \mathbb{R}^m$, $y(t), \hat{y}(t) \in \mathbb{R}^p$, $x(t) \in \mathbb{R}^N$, $\hat{x}(t) \in \mathbb{R}^n$, $n \ll N$
and transfer functions (frequency responses) are close

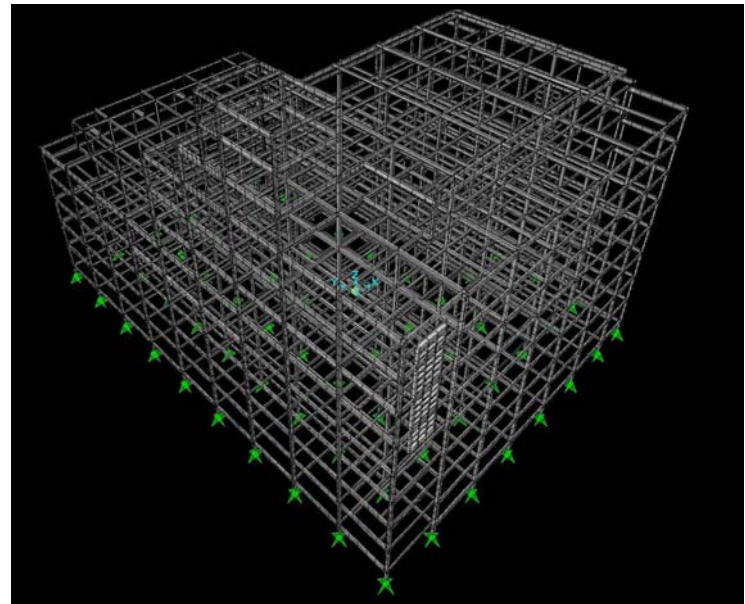
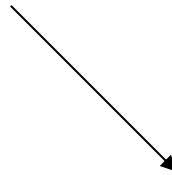
$$\hat{C}(\hat{M}s^2 + \hat{D}s + \hat{S})^{-1}\hat{B} \simeq C(Ms^2 + Ds + S)^{-1}B$$



Start by simplifying the model ...

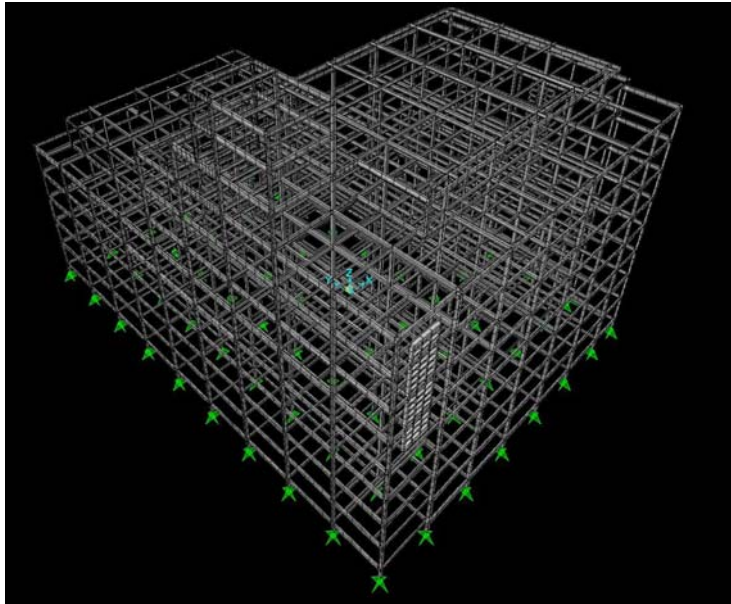


Simplify by
keeping only concrete
substructure

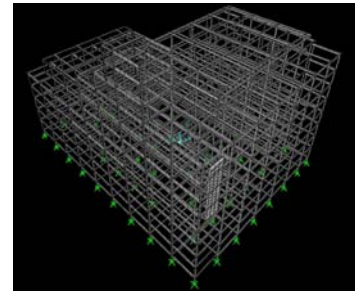


and then reduce the state dimension ...

26400 2nd order eqs



20 2nd order eqs



i.e. reduce the number of equations describing the “state” of the system

Use of 2nd order models

Generalized state space model with $\xi^T(t) = [x^T(t) \quad \dot{x}^T(t)]$

$$\left\{ \begin{array}{l} \underbrace{\begin{bmatrix} D & M \\ M & 0 \end{bmatrix}}_{\mathcal{E}} \dot{\xi}(t) = \underbrace{\begin{bmatrix} -S & 0 \\ 0 & M \end{bmatrix}}_{\mathcal{A}} \xi(t) + \underbrace{\begin{bmatrix} B \\ 0 \end{bmatrix}}_{\mathcal{B}} u(t), \\ y(t) = \underbrace{\begin{bmatrix} C & 0 \end{bmatrix}}_{\mathcal{C}} \xi(t) \end{array} \right.$$

Reduced order model $\{W^*\mathcal{E}V, W^*\mathcal{A}V, W^*\mathcal{B}, \mathcal{C}V\}$ is second order if

$$W = \begin{bmatrix} W_{11} & 0 \\ 0 & W_{22} \end{bmatrix}, \quad V = \begin{bmatrix} V_{11} & 0 \\ 0 & V_{22} \end{bmatrix}$$

Structure constraint on projection spaces !

Clamped beam example

| n | k | m | p | $\frac{\ \mathcal{H} - \tilde{\mathcal{H}}_{BT}\ _2}{\ \mathcal{H}\ _2}$ | $\frac{\ \mathcal{H} - \tilde{\mathcal{H}}_{SOBT}\ _2}{\ \mathcal{H}\ _2}$ |
|-----|----|---|---|--|--|
| 174 | 17 | 1 | 1 | 2.88e-05 | 1.83e-04 |

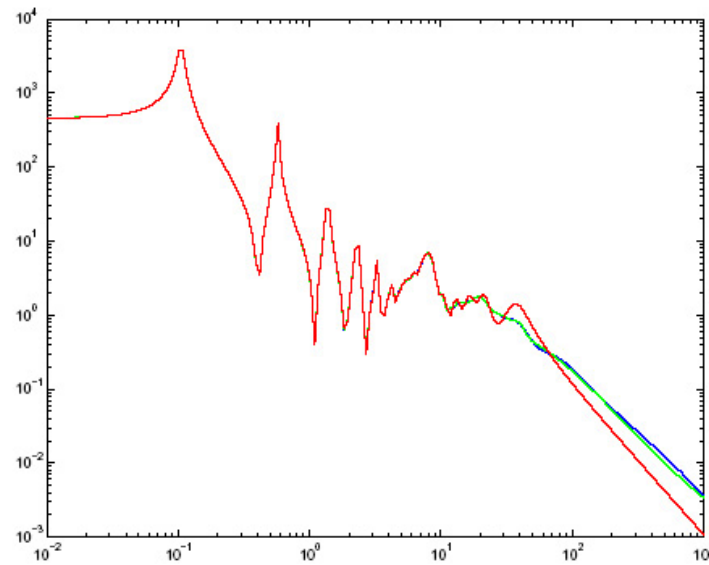
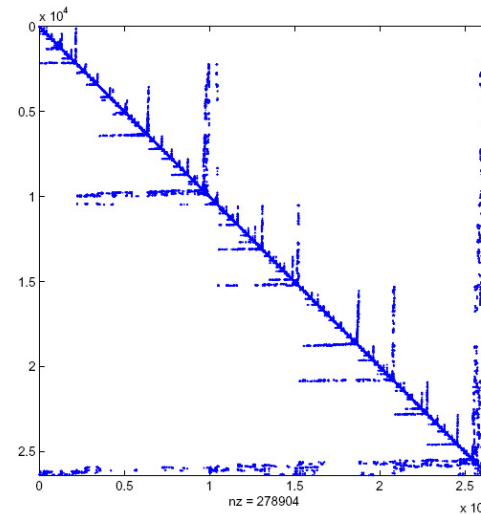


Figure 1: Amplitude of the frequency response.

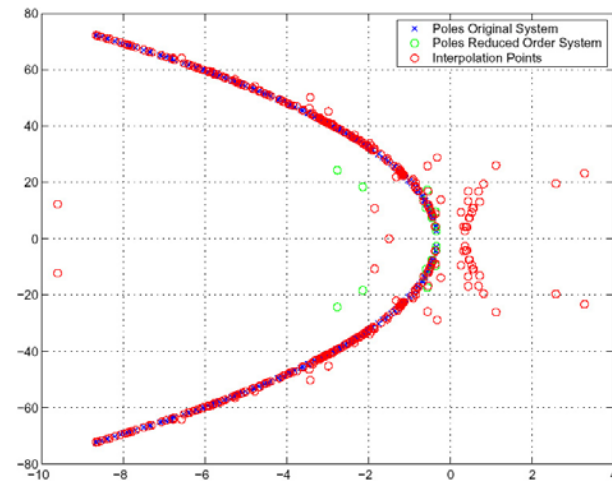
(— Original model, — BT, — SOBT)

Interpolation of large scale systems

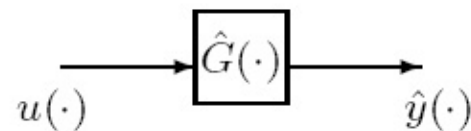
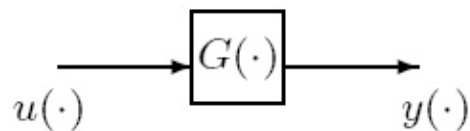
LA hospital building
has 2×26400 variables
but model is sparse



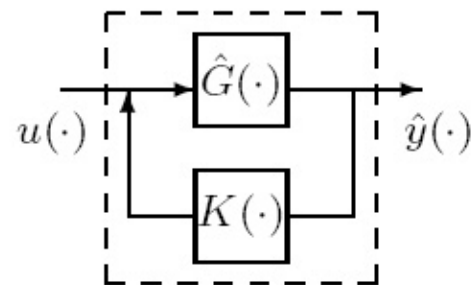
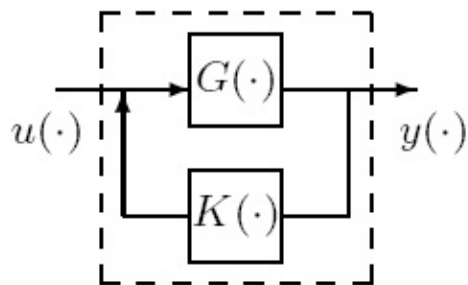
Eigenfrequencies closest
to the origin are typically
good interpolation points



Interconnected systems



Open loop and closed loop approximations can be very different

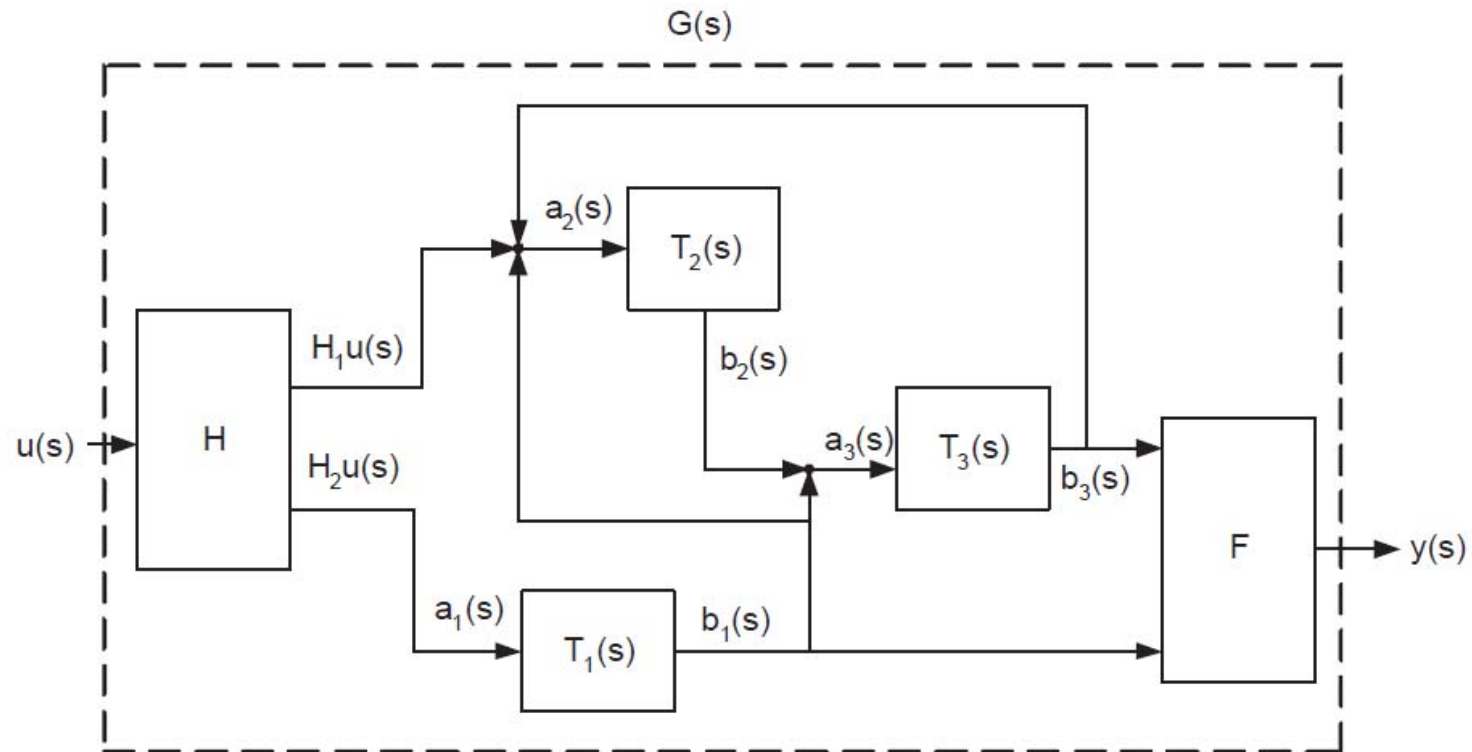


The transfer function is now structured :

$$\min \| (I - G(s)K(s))^{-1}G(s) - (I - \hat{G}(s)K(s))^{-1}\hat{G}(s) \|_{H_\infty}$$

Interconnected systems

$G(s)$ is a set of subsystems $T_i(s)$ that interconnect:



Several examples

Second order systems

$$\mathcal{S} : \begin{cases} (s^2M + sD + S)x(s) &= Bu(s) \\ y(s) &= Cx(s) \end{cases}$$

Cascaded systems

$$\mathcal{S} : y(s) = [W_{out}G(s)W_{in}(s)]u(s)$$

Closed loop systems

$$\mathcal{S} : \begin{bmatrix} y(s) \\ w(s) \end{bmatrix} = \begin{bmatrix} G_{11}(s) & G_{12}(s) \\ G_{21}(s) & G_{22}(s) \end{bmatrix} \begin{bmatrix} u(s) \\ v(s) \end{bmatrix}$$

$$v(s) = C(s)w(s)$$

General interconnected systems

Interconnected systems

$$\begin{bmatrix} w_1(s) \\ \vdots \\ w_k(s) \end{bmatrix} = \begin{bmatrix} G_1(s) & & \\ & \ddots & \\ & & G_k(s) \end{bmatrix} \begin{bmatrix} v_1(s) \\ \vdots \\ v_k(s) \end{bmatrix}$$

Interconnect the components to each other and to the input and output $u(s), y(s)$

$$\begin{bmatrix} v_1(s) \\ \vdots \\ v_k(s) \end{bmatrix} = \begin{bmatrix} K_{11} & \dots & K_{1k} \\ \vdots & \ddots & \vdots \\ K_{k1} & \dots & K_{kk} \end{bmatrix} \begin{bmatrix} w_1(s) \\ \vdots \\ w_k(s) \end{bmatrix} + \begin{bmatrix} H_1 \\ \vdots \\ H_k \end{bmatrix} u(s)$$
$$y(s) = \begin{bmatrix} F_1 & \dots & F_k \end{bmatrix} \begin{bmatrix} w_1(s) \\ \vdots \\ w_k(s) \end{bmatrix}$$

Realize interconnected systems

Realize $G_i(s)$ of McMillan degree n_i as $C_i(sI_{n_i} - A_i)^{-1}B_i + D_i$ yielding :

$$A := \text{diag}\{A_i\}, \quad B := \text{diag}\{B_i\}, \quad C := \text{diag}\{C_i\}, \quad D := \text{diag}\{D_i\},$$

The interconnected system $T(s)$ is then realized by :

$$\begin{aligned} A_T &:= A + BK(I - DK)^{-1}C, & B_T &:= B(I - KD)^{-1}H, \\ C_T &:= F(I - DK)^{-1}C, & D_T &:= FD(I - KD)^{-1}H \end{aligned}$$

It is not as bad as it looks since K is typically sparse, which is maintained in the realization of $T(s)$

Example

Weighted systems:

$$\mathcal{S} : \begin{cases} w_1(s) = W_o(s)v_1(s), & w_2(s) = G(s)v_2(s), & w_3(s) = W_i(s)v_3(s) \\ y(s) = w_1(s), & v_1(s) = w_2(s), & v_2(s) = w_3(s), & v_3 = u(s) \end{cases}$$

Cascaded system realized by

$$\left[\begin{array}{ccc|c} A_o & B_oC & B_oDC_i & B_oDD_i \\ & A & BC_i & BD_i \\ & & A_i & B_i \\ \hline C_o & D_oC & D_oDC_i & D_oDD_i \end{array} \right]$$

Closed loop Gramians

Idea: For each subsystem $G_i(s)$, define $n_i \times n_i$ Gramians containing information about the energy distribution of the I/O map in x_i **only**.

Let us consider the controllability and observability Gramians of $T(s)$:

$$A_T P_T + P_T A_T^T + B_T B_T^T = 0 \quad , \quad A_T^T Q_T + Q_T A_T + C_T^T C_T = 0.$$

Decompose, with $P_{ij}, Q_{ij} \in \mathbb{C}^{n_i \times n_j}$

$$P_T = \begin{bmatrix} P_{11} & \dots & P_{1k} \\ \vdots & \ddots & \vdots \\ P_{k1} & \dots & P_{kk} \end{bmatrix} \quad , \quad Q_T = \begin{bmatrix} Q_{11} & \dots & Q_{1k} \\ \vdots & \ddots & \vdots \\ Q_{k1} & \dots & Q_{kk} \end{bmatrix} ,$$

Constrained Gramians

Energy interpretation of diagonal blocks $[P_{ii}]^{-1}$ and $[P^{-1}]_{ii}$

$$\min_{u, \bigcup_{j \neq i} x_j(0)} \|u(-\infty, 0)\|_{\mathcal{L}_2}^2 = x_i(0)^T [P_{ii}]^{-1} x_i(0)$$

$$\min_{u, \forall_{j \neq i} x_j(0)=0} \|u(-\infty, 0)\|_{\mathcal{L}_2}^2 = x_i(0)^T [P^{-1}]_{ii} x_i(0)$$

Similar for diagonal blocks $[Q_{ii}]^{-1}$ and $[Q^{-1}]_{ii}$

(see Enns, Liu, Varga, VV...)

Constrained Krylov spaces

If

$$(\hat{A}, \hat{B}, \hat{C}) = (Z^T A V, Z^T B, C V), \quad Z^T V = I$$

where

$$\mathcal{K}_k((\sigma I - A)^{-1}, (\sigma I - A)^{-1} B) \subseteq \text{Im}(V)$$

Then

$$(\hat{A}_T, \hat{B}_T, \hat{C}_T) = (Z^T A_T V, Z^T B_T, C_T V), \quad Z^T V = I$$

and

$$\mathcal{K}_k((\sigma I - A_T)^{-1}, (\sigma I - A_T)^{-1} B_T) \subseteq \mathcal{K}_k((\sigma I - A)^{-1}, (\sigma I - A)^{-1} B)$$

Open loop equals closed loop interpolation unless you change points !?

Time-varying linear systems

Approximate the (discrete) time-varying systems

$$\begin{cases} x(k+1) = A(k)x(k) + B(k)u(k) \\ y(k) = C(k)x(k) + D(k)u(k) \end{cases}$$

by a lower order models of same type. We notice that

$$\begin{bmatrix} y(k) \\ y(k+1) \\ y(k+2) \\ \vdots \end{bmatrix} = \begin{bmatrix} C(k) \\ C(k+1)A(k) \\ C(k+2)A(k+1)A(k) \\ \vdots \end{bmatrix} x(k),$$

$$x(k) =$$

$$\begin{bmatrix} B_{(k-1)} & A_{(k-1)}B_{(k-2)} & A_{(k-1)}A_{(k-2)}B_{(k-3)} & \dots \end{bmatrix} \begin{bmatrix} u(k-1) \\ u(k-2) \\ u(k-3) \\ \vdots \end{bmatrix}$$

H_2 approximation

Systems now look like

$$\begin{cases} x_{k+1} &= A_k x_k + B_k u_k \\ y_k &= C_k x_k \end{cases} \quad \begin{cases} \hat{x}_{k+1} &= \hat{A}_k \hat{x}_k + \hat{B}_k u_k \\ \hat{y}_k &= \hat{C}_k \hat{x}_k \end{cases}$$

with an error system where $e_k := y_k - \hat{y}_k$

$$\mathcal{E} := \begin{cases} x_{k+1}^e &= A_k^e x_k^e + B_k^e u_k \\ e_k &= C_k^e x_k^e \end{cases}$$

where

$$A_k^e := \begin{bmatrix} A_k & \\ & \hat{A}_k \end{bmatrix}, \quad B_k^e = \begin{bmatrix} B_k \\ \hat{B}_k \end{bmatrix}, \quad C_k^e = [C_k - \hat{C}_k]$$

Its state for initial condition $x_{k_0}^e = 0$ is given by

$$x_k^e = \sum_{i=k_0}^{k-1} \Phi_{k,i+1}^e B_i^e u_i, \quad \Phi_{k+1,i}^e = A_k^e \Phi_{k,i}^e \quad (k \geq i), \quad \Phi_{k,k}^e = I$$

Error function is a linear map

Error system response satisfies

$$\tilde{e} = E\tilde{u}, \quad \tilde{e} := \begin{bmatrix} e_{k_0+1} \\ \vdots \\ e_{k_f+1} \end{bmatrix}, \quad \tilde{u} := \begin{bmatrix} u_{k_0} \\ \vdots \\ u_{k_f} \end{bmatrix}, \quad E = D_C H D_B$$

and

$$D_C = \begin{bmatrix} C_{k_0+1}^e & & 0 \\ & \ddots & \\ 0 & & C_{k_f+1}^e \end{bmatrix}, \quad D_B = \begin{bmatrix} B_{k_0}^e & & 0 \\ & \ddots & \\ 0 & & B_{k_f}^e \end{bmatrix}$$
$$H = \begin{bmatrix} \Phi_{k_0, k_0}^e & & 0 \\ \vdots & \ddots & \\ \Phi_{k_f, k_0}^e & \cdots & \Phi_{k_f, k_f}^e \end{bmatrix}$$

depends on the reduced order model

$$\|\mathcal{E}\|_{\mathcal{H}_2}^2 := \mathcal{J}(k_0, k_f) := \text{tr}(E^T E) = \text{tr}(E E^T)$$

One shows that

$$\mathcal{J}(k_0, k_f) := \text{tr} \sum_{k=k_0+1}^{k_f+1} C_k^e P_k^e C_k^{e^T} = \text{tr} \sum_{k=k_0}^{k_f} B_k^{e^T} Q_k^e B_k^e$$

where

$$P_{k+1}^e = \begin{bmatrix} A_k & \\ & \hat{A}_k \end{bmatrix} P_k^e \begin{bmatrix} A_k^T & \\ & \hat{A}_k^T \end{bmatrix} + \begin{bmatrix} B_k \\ \hat{B}_k \end{bmatrix} \begin{bmatrix} B_k^T & \hat{B}_k^T \end{bmatrix}$$
$$Q_{k-1}^e = \begin{bmatrix} A_k^T & \\ & \hat{A}_k^T \end{bmatrix} Q_k^e \begin{bmatrix} A_k & \\ & \hat{A}_k \end{bmatrix} + \begin{bmatrix} C_k^T \\ \hat{C}_k^T \end{bmatrix} \begin{bmatrix} C_k & \hat{C}_k \end{bmatrix},$$

[VD-Gallivan-Absil, CESAME rept., Univ. Cath. Louvain, 2009]

Gradients are given by

$$\nabla_{\hat{A}_k} \mathcal{J} = 2(\hat{Q}_k \hat{A}_k \hat{P}_k + Y_k^T A_k X_k),$$

$$\nabla_{\hat{B}_k} \mathcal{J} = 2(\hat{Q}_k \hat{B}_k + Y_k^T B_k),$$

$$\nabla_{\hat{C}_k} \mathcal{J} = 2(\hat{C}_k \hat{P}_k - C_k X_k)$$

Updating rules and fixed point results are as before

$$W_k := Y_k \hat{Q}_k^{-1}, V_k = X_k \hat{P}_k^{-1}$$

$$(A_k^e, B_k^e, C_k^e) := (W_k^T A_k V_k, W_k^T B_k, C_k V_k).$$

where $X_k, Y_k, \tilde{P}_k, \tilde{Q}_k$ satisfy Stein like recurrences

$$X_{k+1} = A_k X_k \hat{A}_k^T + B_k \hat{B}_k^T,$$

$$\hat{P}_{k+1} = \hat{A}_k \hat{P}_k \hat{A}_k^T + \hat{B}_k \hat{B}_k^T,$$

$$Y_{k-1} = A_k^T Y_k \hat{A}_k^T - C_k^T \hat{C}_k,$$

$$\hat{Q}_{k-1} = \hat{A}_k^T \hat{Q}_k \hat{A}_k + \hat{C}_k^T \hat{C}_k,$$

Nonlinear systems

Look for a simple energy function

Consider the discrete-time system

$$\begin{cases} x(k+1) = G(x(k), u(k)) \\ y(k) = H(x(k), u(k)). \end{cases}$$

One could linearize along a “nominal” trajectory $(x(k), u(k))$
and get $A(\cdot), B(\cdot), C(\cdot), D(\cdot)$ from Taylor expansion of $G(\cdot, \cdot), H(\cdot, \cdot)$

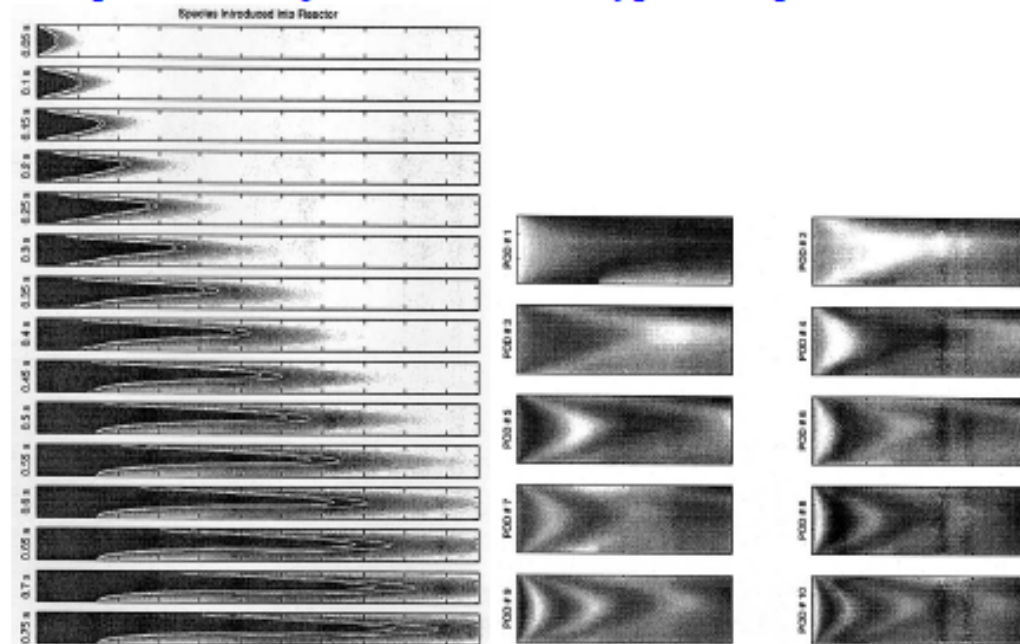
Simpler idea (POD) : (Holmes-Lumley-Berkooz '96)

Use the “energy function” $G \doteq \sum_{k=k_i}^{k_f} x(k)x(k)^T$.

Example

Chemical vapor deposition reactor

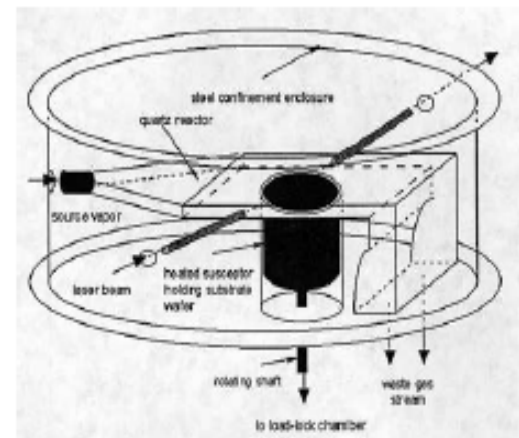
Compute state trajectories for one “typical” input :



Snap shots of “typical” states

Ten dominant “states”

Use POD in CVD reactor (Ly-Tran '99)



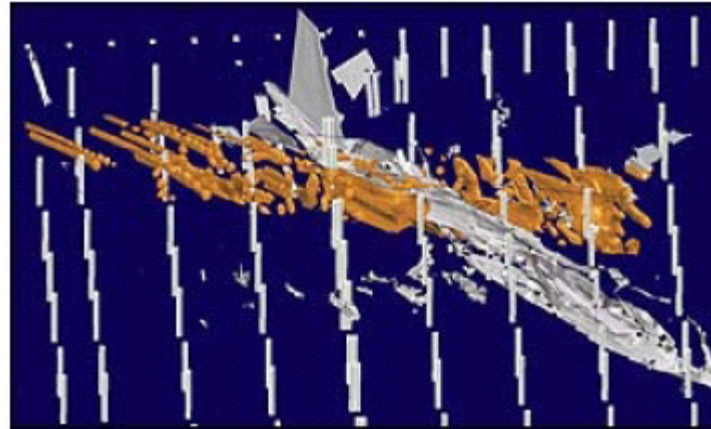
Schematic representation of a horizontal quartz reactor in a steel confinement shell

Conclusions

- Model reduction of linear time invariant systems is quite sophisticated and efficient these days
- Algorithmic aspects are the issue right now
- Time-varying extensions exist (for discrete-time case)
- Nonlinear extensions exist but lack well established results
- There are many successful test cases
- Model reduction is stil quite hot ...

BBC report
of Sept. 2002

Computer clues to Pentagon attack



Orange shows fuel onboard as the plane crashed

A computer simulation of the attack against the Pentagon last September could be used to design buildings that can withstand terrorist attacks.

The software used principles of physics to show how the plane's huge mass of fuel and cargo impacted the building.

It could help design buildings such as hospitals and fire stations that would be more resistant to similar attacks.