



Finite Element Method for fluid flow problems in an industrial R&D context - Motivations, theory and applications

Cenaero's intervention in UCLouvain's course *Introduction aux éléments finis (LEPL1110)* Teacher: Vincent Legat

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Context – Why numerical simulations matter



FEM for fluid flow equation

2 Cer

Context – Numerical simulations is one of the pillars of predictive science



Context – Challenges and requirements for simulating fluid flows



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Context – Challenges and requirements for simulating fluid flows

Challenges

Multiphysics nature -> stiffness

Bow Shear Shock Ablation Product Layer Contamination Viscous Interaction Afterbody Hea Separation Shock Layer RCS Radiation Interaction Dissociation & Ionization Recompression Ro Surface Recombination Ablation & Recession Continuum Boundary Layer Breakdowr Transition Separation Credit : NASA









Credits: [1] Schrooyen PhD thesis, UCLouvain; 2015

FEM for fluid flow equation

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5 Cenaer

Outline

| <u>Challenges</u> | | <u>Method</u> requirements |
|---|---|-------------------------------|
| Complex geometries | Element-based spatial discretization | Flexibility |
| Margaux's talk | | |
| Wide range of scales | High-order spatial discretization | High-resolution |
| Non-linearities -> singularities | FEM vs Discontinuous Galerkin | Stability |
| Multiphysics nature + high-order operators -> stiffness | Full discrete system solving | Robustness |
| Computational cost | Marg Exploitation of high-fidelity results for machine learning | aux's talk Efficiency |

FEM for fluid flow equation

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Prototype advection-diffusion equation – strong form

$$\tilde{\mathbf{u}} \in \tilde{\mathcal{U}} \qquad \frac{\partial \tilde{\mathbf{u}}}{\partial t} + \tilde{\nabla} \cdot (c \, \tilde{\mathbf{u}}) - \tilde{\nabla} \cdot (d \, \tilde{\nabla} \tilde{\mathbf{u}}) = \mathbf{0} \quad \text{on } \tilde{\Omega}$$

You've seen that for elliptic problem (c=0, u(x)): FEM <=> functional minimization

$$J(\tilde{\mathbf{u}}) = \min_{\tilde{\mathbf{w}} \in \tilde{\mathcal{U}}} J(\tilde{\mathbf{w}})$$

 But breaks down for hyperbolic equation => go for the more general weighted residual approach

Pointwise condition -> KO for non-smooth solution Integral ("average") condition -> OK for non-smooth solution (derivatives in the sense of distributions)



- Discretization: from infinite space to 'computer-compatible' finite space
 - $\circ~$ On the domain (meshing): $~~\Omegapprox~\widetilde{\Omega}~$
 - On the test functions:

$$\widetilde{\mathbf{w}} \in C^{\infty}_{\mathcal{C}}(\widetilde{\Omega}) \longrightarrow \mathbf{W} \in \mathcal{W} \coloneqq \operatorname{span}\{\mathbf{w}_{1}, \dots, \mathbf{w}_{n}, \dots, \mathbf{w}_{N_{n}}\}$$
$$\int_{\widetilde{\Omega}} \widetilde{\mathcal{R}} [\widetilde{\mathbf{u}}] \ \widetilde{\mathbf{w}} \, \mathrm{d}\mathbf{x} = \mathbf{0} \longrightarrow \int_{\widetilde{\Omega}} \widetilde{\mathcal{R}} [\widetilde{\mathbf{u}}] \ \mathbf{w}_{n} \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots, N_{n}$$

• On the trial functions:

$$\widetilde{\mathbf{u}} \in \widetilde{\mathcal{U}} \subset \mathcal{C}^2(\widetilde{\Omega}) \longrightarrow \mathbf{u} \in \mathcal{U} \coloneqq \operatorname{span}\{\phi_1, \dots, \phi_m, \dots, \phi_{N_m}\}$$
$$\longrightarrow \int_{\Omega} \mathcal{R}[\mathbf{u}] \ \mathbf{w}_n \ \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots, N_n$$

We seek an approximate solution such that the residual of the equations is made "small" in a certain integral sense (but not = 0 anymore due to discretization)

$$\mathcal{R}[\mathbf{u}] \neq \tilde{\mathcal{R}}[\tilde{\mathbf{u}}] = \mathbf{0}$$



Discretization through the weighted residual perspective





- Method choice:
 - Weighting of the residual





Outline



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12 Cei

Sources of numerical errors





Sources of numerical errors

Approximation error: truncation of expansion

$$\tilde{\mathbf{u}}(\mathbf{x}) = \sum_{i=0}^{\infty} \hat{\tilde{\mathbf{U}}}_i \, \xi_i(\mathbf{x}) \quad \longrightarrow \quad \mathbf{u}(\mathbf{x}) = \sum_{i=0}^{N} \hat{\mathbf{U}}_i \, \xi_i(\mathbf{x})$$
$$\epsilon_1 = \sum_{i=N+1}^{\infty} \hat{\tilde{\mathbf{U}}}_i \, \xi_i(\mathbf{x})$$

PDE discretization error: discrete weighted residual formulation

$$\mathcal{R}[\mathbf{u}] \neq \tilde{\mathcal{R}}[\tilde{\mathbf{u}}] = \mathbf{0} \implies \epsilon_{2,i} = |\hat{\mathbf{U}}_i - \hat{\mathbf{U}}_i| \quad i = 0, \dots, N$$

For non-linear problem, those discretization errors interact across the scales -> aliasing errors may accumulate energy in the high modes and affect the lower modes



• Approximation and discretization errors lead to alterations of phase (dispersion) and amplitude (dissipation) of the signal (solution)

$$\epsilon_1 = \sum_{i=N+1}^{\infty} \hat{\mathbf{U}}_i \xi_i(\mathbf{x}) \quad \square \quad \epsilon_{2,i} = |\hat{\mathbf{U}}_i - \hat{\mathbf{U}}_i| \quad i = 0, \dots, N$$



[1] https://hplgit.github.io/fdm-book/doc/pub/book/sphinx/._book012.html

Increasing the scheme order reduces dispersion and dissipation errors ->
increased resolution capabilities at higher modes





[1] Kadanoff, Leo P. "Excellence in computer simulation. " *Computing in Science & Engineering* 6.2 (2004) 57-67.

Why going high-order can pay off

 $\mathbf{u}(\mathbf{x}) =$

 $\mathbf{U}_m \, \phi_m(\mathbf{x})$

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17

- FE-type element-based methods offer a natural way to improve subcell resolution by locally increasing the interpolation order (i.e. without stencil extension)
- For the same # DOF, increasing the order quickly leads to errors levels (far) below what can mesh refinement reaches





[1] Wang, Zhi Jian. "High-order methods for the Euler and Navier– Stokes equations on unstructured grids." *Progress in Aerospace Sciences* 43.1-3 (2007): 1-41.

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18

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- You've seen that the coercivity (hence stability) of the continuous FE • discretized form is ensured for pure elliptic problem.
- But it's note the case for hyperbolic problem -> let's consider that case:

$$\mathsf{R}[\tilde{\mathbf{u}}] \coloneqq \tilde{\nabla} \cdot (c \, \tilde{\mathbf{u}}) = \mathbf{0} \quad \text{on } \tilde{\Omega} \quad \Longrightarrow \quad \int_{\Omega} \mathscr{R}[\mathbf{u}] \, \mathbf{w}_n \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_n$$

Different choices of function space between FEM and DGM:



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$$\mathcal{R}[\mathbf{u}] \mathbf{w}_n \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_n$$

• Galerkin continuous FE (with weak essential boundary condition enforcement)

$$\int_{\Omega} \left[\nabla \cdot (c \, u) \right] w \, \mathrm{d}x + \int_{\partial \Omega} c(u - u_B) w \, \mathrm{d}s = 0 \,, \quad \forall w \in \mathcal{W}_p^c$$

 The form is coercive... but not in the norm defining the function space -> no control leading to oscillatory solution as the mesh is refined

$$B(v,v) \ge \gamma_0 \int_{\Omega} w^2 \, \mathrm{d}x + \frac{1}{2} \int_{\partial \Omega} b \, w^2 \, \mathrm{d}s$$



$$\mathcal{R}[\mathbf{u}] \mathbf{w}_n \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_n$$

Petrov-Galerkin continuous FE (with weak essential boundary condition enforcement)

$$\int_{\Omega} \left[\nabla \cdot (c \, u) \right] \left[w + c \, \zeta \, \nabla w \right] \, \mathrm{d}x + \int_{\partial \Omega} c (u - u_B) w \, \mathrm{d}s = 0 \,, \quad \forall w \in \mathcal{W}_p^c$$

 Artificial diffusion in streamline direction "c" gives now control on the previously unbounded directional derivative of the solution

$$\zeta \int_{\Omega} (c \,\nabla u) (c \,\nabla w) \,\mathrm{d}x + \zeta \int_{\Omega} (\nabla c \,u) (c \,\nabla w) \,\mathrm{d}x$$



$${}_{\Omega} \mathcal{R}[\mathbf{u}] \mathbf{w}_n \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_n$$

• Discontinuous Galerkin FE

$$\int_{\mathbf{T}_m} \left[\nabla \cdot (c \, u) \right] w \, \mathrm{d}x = 0 \xrightarrow{\text{Integration by part}} - \int_{\mathbf{T}_m} (c \, u) \nabla w \, \mathrm{d}x + \int_{\partial \mathbf{T}_m} c \, u \, w \, \mathrm{d}s = 0$$
$$- \int_{\Omega} (c \, u) \nabla w \, \mathrm{d}x + \sum_{\mathbf{T}_m} \int_{\partial \mathbf{T}_m} \underbrace{c \, u}_{\mathcal{F}} w \, \mathrm{d}s = 0 \,, \quad \forall w \in \mathcal{W}_p^d \xleftarrow{\text{Sum over elements}} e_{\text{elements}}$$



$$\mathcal{R}[\mathbf{u}] \mathbf{w}_n \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_n$$

• Discontinuous Galerkin FE

• Because of solution jump at element interfaces, definition of a numerical flux function based on left and right states

• Control on the solution jump in the DG norm only if b 0 = 0. $\mathcal{F} = \begin{cases} b u^- & \text{if } b < 0 \\ b u^+ & \text{if } b \ge 0 \end{cases}$ In particular, upwind stabilization is ensured by $b_0 = \frac{1}{2}|b|$

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$$\bigcap_{\Omega} \mathcal{R}[\mathbf{u}] \mathbf{w}_n \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_n$$

 Discontinuous Galerkin FE exploits weak imposition of inter-element continuity, in contrast to strong continuity in continuous FEM. This has a stabilizing effect (if numerical flux properly chosen) and lead to improved order of convergence.

$$\int_{\Omega} \left[\nabla \cdot (c \, u) \right] w \, \mathrm{d}x - \sum_{\mathbf{T}_m \setminus \partial \Omega} \int_{\partial \mathbf{T}_m} c(u^+ - u^-) w \, \mathrm{d}s + \int_{\partial \Omega} c(u - u_B) w \, \mathrm{d}s = 0 \,, \quad \forall w \in \mathcal{W}_p^c$$

 What about elliptic operator with DGM? Contrary to continuous FEM, wellposedness via the Lax-Milgram theorem cannot be invoked since we're considering non-conforming FE -> need to prove it for every discrete function space (i.e. stability conditions depending on element type and order).



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Application of DG spatial discretization to Navier-Stokes fluid equations

 Also an advection-diffusion-reaction equation on which we apply weighted residual approach

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot \underline{F}^{c}(\mathbf{u}) = \nabla \cdot \underline{F}^{d}(\mathbf{u}, \nabla \mathbf{u}) + \mathbf{S}(\mathbf{u}, \nabla \mathbf{u}) \longrightarrow \tilde{\mathcal{R}} [\tilde{\mathbf{u}}] \triangleq \frac{\partial \tilde{\mathbf{u}}}{\partial t} + \tilde{\nabla} \cdot \underline{F}(\tilde{\mathbf{u}}, \tilde{\nabla}\tilde{\mathbf{u}}) - \mathbf{S}(\tilde{\mathbf{u}}, \tilde{\nabla}\tilde{\mathbf{u}}) = \mathbf{0}$$
$$\int_{\Omega} \mathcal{R}[\mathbf{u}] \mathbf{w}_{n} \, \mathrm{d}\mathbf{x} = \mathbf{0} \quad \text{for } n = 1, \dots N_{n}$$

DG discerization leads to a system of ODEs to be integrated in time



Application of DG spatial discretization to Navier-Stokes fluid equations

$$\underbrace{\sum_{m\in\mathbb{T}}\int_{\mathbb{T}_m}\boldsymbol{\phi}_{m,-}\boldsymbol{\phi}_{m,-}^T\,\mathrm{d}\mathbf{x}}_{\underline{M}} \,\frac{\mathrm{d}\underline{\boldsymbol{U}}_{-,-,-}}{\mathrm{d}t} + \mathcal{N}^{\mathrm{sp}}(\underline{\boldsymbol{U}}_{-,-,-}) = 0$$

Unsteady Explicit

$$\mathcal{N}^{\mathrm{tp}}(\mathbf{U}(t_{n+1})) + \mathcal{N}^{\mathrm{sp}}(\mathbf{U}(t_n)) = \mathbf{0}$$

 Linear temporal term -> solution at next time step directly available Time-marching steady or unsteady Implicit

 $\mathcal{N}^{\mathrm{tp}}(\mathbf{U}(t_{n+1})) + \mathcal{N}^{\mathrm{sp}}(\mathbf{U}(t_{n+1})) = \mathbf{0}$

- Non-linear system to solve at each time step
- Linear system to solve at each iteration







- Advantages
 - Ability to handle complex geometries
 - Guaranteed order of convergence p+1 on unstructured meshes
 - No degradation near size jumps/walls



31 Cenaei

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32 Cenaei

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 - Good dispersion-dissipation properties



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 - hp-adaptation



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 - Shared operations (parametric)
 - Local operations
 - Low transfer work and operation hiding possible (parallel efficiency)



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 - Low transfer work and operation hiding possible (parallel efficiency)
 - Local conservation
- Drawbacks
 - Duplication of the degrees of freedom on the element boundaries (costly)
 - Sensitive to under-resolved features



• Hartmann, Ralf. "Numerical analysis of higher order discontinuous Galerkin finite element methods." (2008)



Applications - Detailed thermo-chemical degradation study of critical space debris materials

Argo flow solver (steady state) coupled with Argo Material solver (unsteady simulation with immersed method)

- Mostly used for melting materials (coupled with hydrodynamic conservation laws)
- Staggered approach exploits the difference in time scale for flow/material response

Argo flow solver accounting for the presence of reacting porous material (unified method)

 Use of volume averaging method to develop single set of equations valid for low/dense reactive porous materials



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Outline



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41 Cer