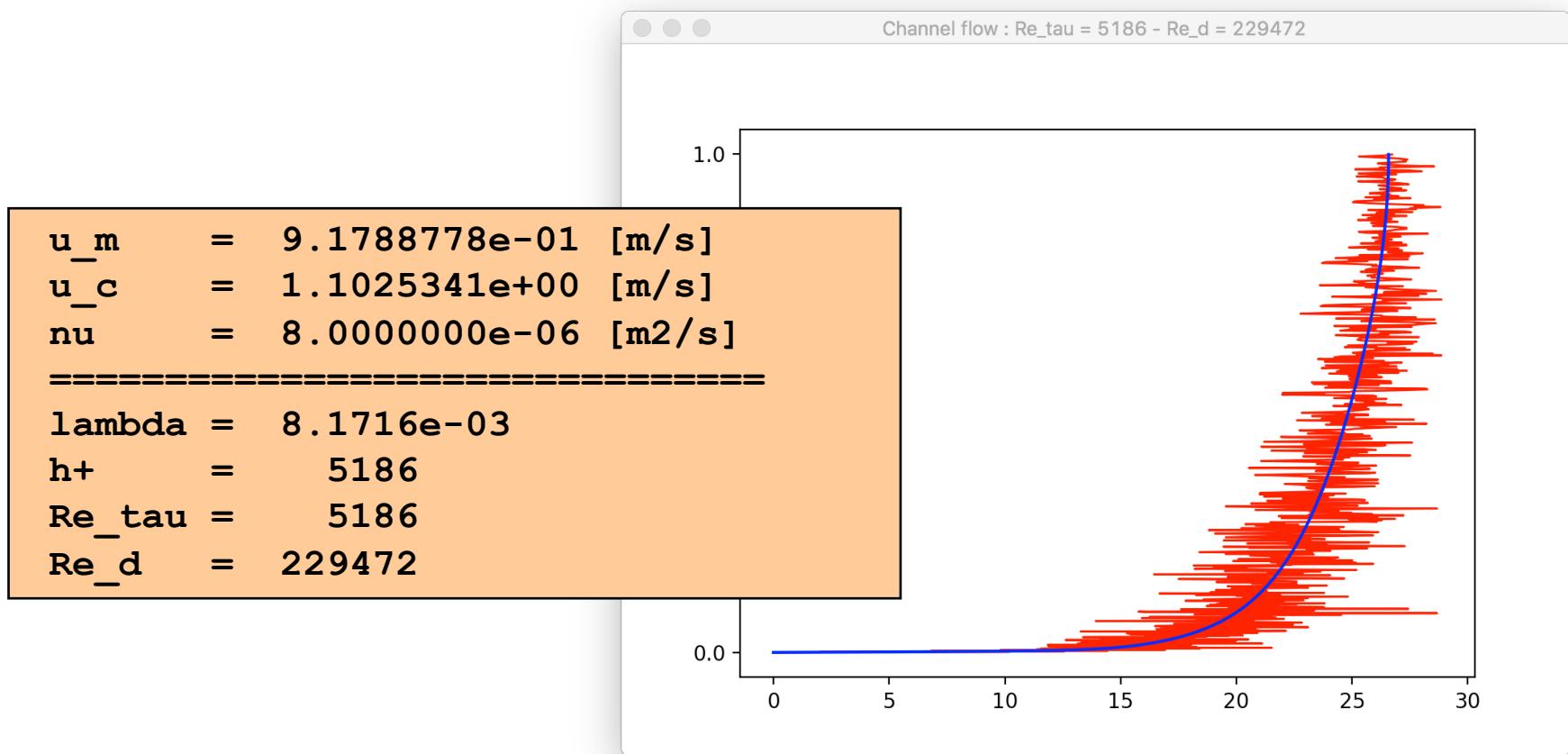


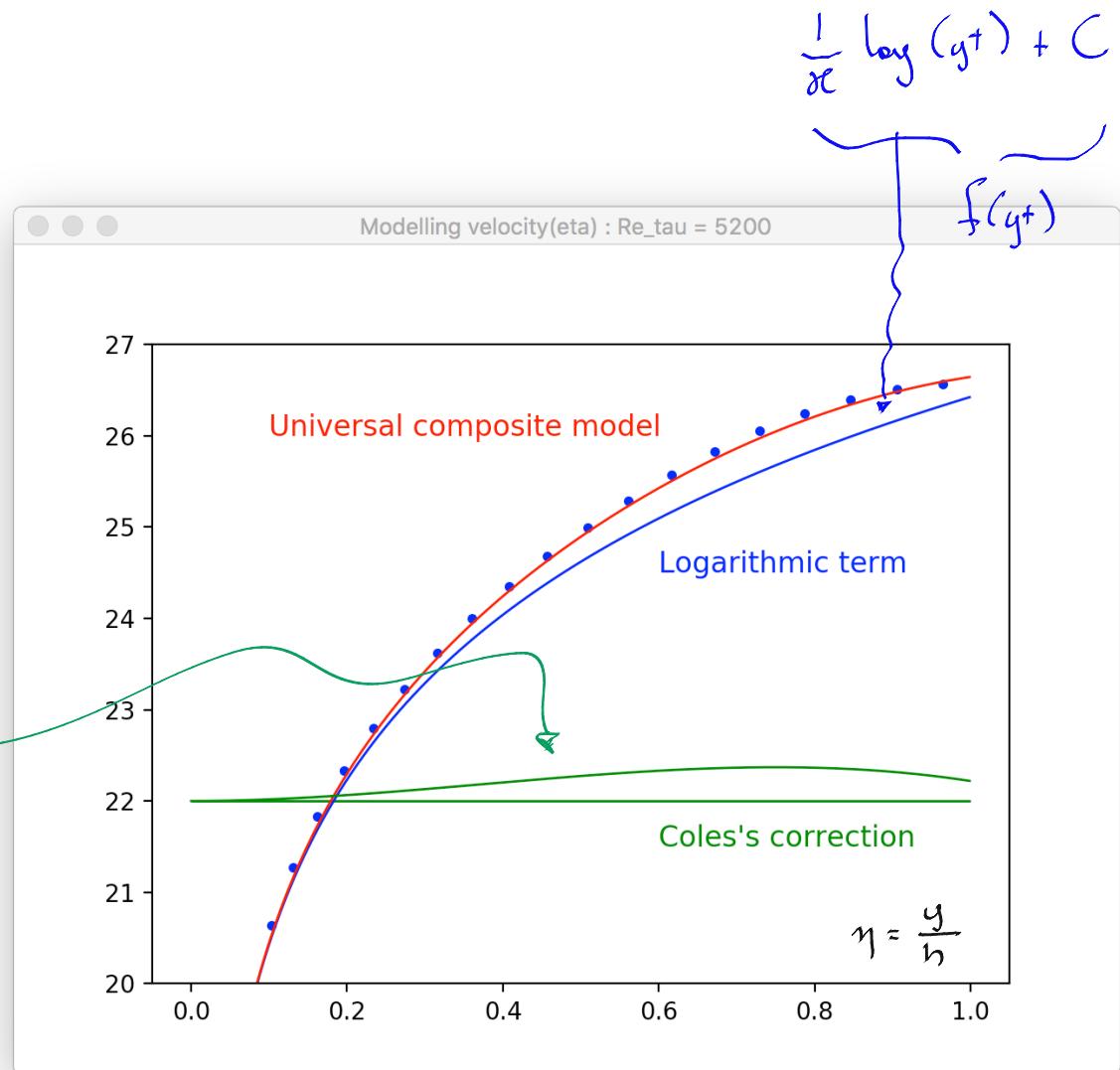
Pertes de charges turbulentes



Ecoulement en canal

$$D \left[3(\alpha\eta)^2 - 2(\alpha\eta)^3 \right]$$

$$G(\eta)$$

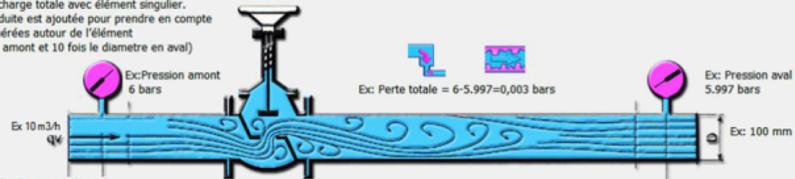


Profil logarithmique ===== kappa = 0.3840 et C = 4.1500
Correction de Coles ===== alpha = 1.3333 et D = 0.3700

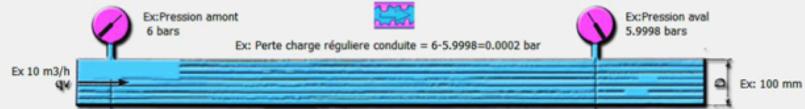
La formule des ingénieurs

Méthode de mesure expérimentale des coefficients de pertes de charge:

1: Mesurer la perte de charge totale avec élément singulier.
Une longueur de conduite est ajoutée pour prendre en compte les perturbations générées autour de l'élément
(2fois le diamètre en amont et 10 fois le diamètre en aval)



2: Mesurer de la perte de charge régulière de la longueur de conduite ajoutée(égale à 12 fois le diamètre)



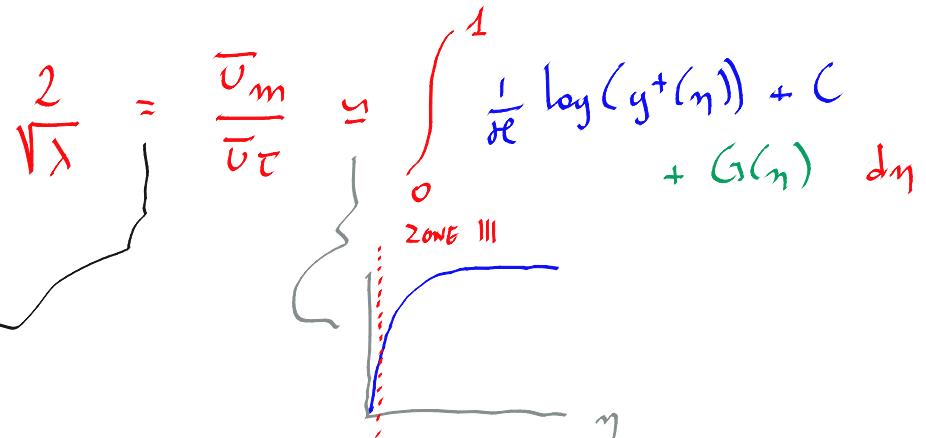
3: Calcul du coefficient de perte de charge singulière:
Perte singulière= perte totale - perte régulière = Exemple: 0.003bars-0.0002bars = 0.0028 bars = 0.0028 X100 000 = 280 pascals
Section m² = (Diamètre_m/2)² x 3.1416 = Ex: (0,1/2)²x3.14=0.0025x3.14=0.00785m²
Qv m³_sec= débit m³/h/3600 = Ex: 10 m3/h / 3600 = 0.002777 m³_sec
Vitesse_fluide_m_sec = Qv/débit volumique en m³_sec / Section_m² = Ex: 0.002777/0.00785 = 0.35 m/sec
Pression dynamique(pascals) = 0.5 x masse_volumique_kgm3 x (Vitesse_fluide_m_sec)²= Ex: avec eau, = 0.5 x 1000 x 0.35²=61.25 pascals
Coefficient de pertes de charges singulière = Perte singulière(pascals)/Pression dynamique(pascals) = Ex: 61.25/ 280 = 0.218

$$\frac{1}{\sqrt{\lambda}} = -a \log_{10} \left(\frac{b}{Re_d} \frac{1}{\sqrt{\lambda}} \right)$$

$$Re_d = \frac{2h\bar{u}_m}{\nu}$$

$$Re_\tau = \frac{h\bar{u}_\tau}{\nu} = h^+$$

Un peu d'algèbre un brin fastidieuse



$$= \int_0^2 \frac{1}{\delta e} \log \left[\underbrace{\frac{h \bar{v}_T}{h^+}}_{h^+} \underbrace{\frac{y}{\eta}}_{\eta} \right] + C + D \left[3(\alpha \eta)^2 - 2(\alpha \eta)^3 \right] d\eta$$

$\log(h^+) + \log(\eta)$

$$= \frac{1}{\delta e} \log(h^+) + C + \frac{1}{\delta e} \int_0^1 \log \eta \, d\eta + D \left[\underbrace{\frac{3\alpha^2 \eta^3}{3} - \frac{2\alpha^3 \eta^4}{4}}_{\alpha^2 - \alpha^3/2} \right]_0^1$$

$(\eta \log \eta)' = \log \eta + 1$

$[\eta \log \eta - \eta]_0^1 = -1$

$$\frac{2}{\sqrt{x}} = \frac{1}{\alpha} \log(h^+) + C + \frac{1}{\alpha} \int_0^x \log n \, dn + D \left[\frac{3\alpha^2 n^3}{3} - \frac{2\alpha^3 n^4}{4} \right]_0^1$$

$(n \log n)' = \log n + 1$

$\left[n \log n - n \right]_0^1 = -1$

$\alpha^2 - \alpha^3/2$

$$= \frac{1}{\alpha} \log(h^+) + \left[C - \frac{1}{\alpha} + D(\alpha^2 - \frac{1}{2}\alpha^3) \right]$$

[?]

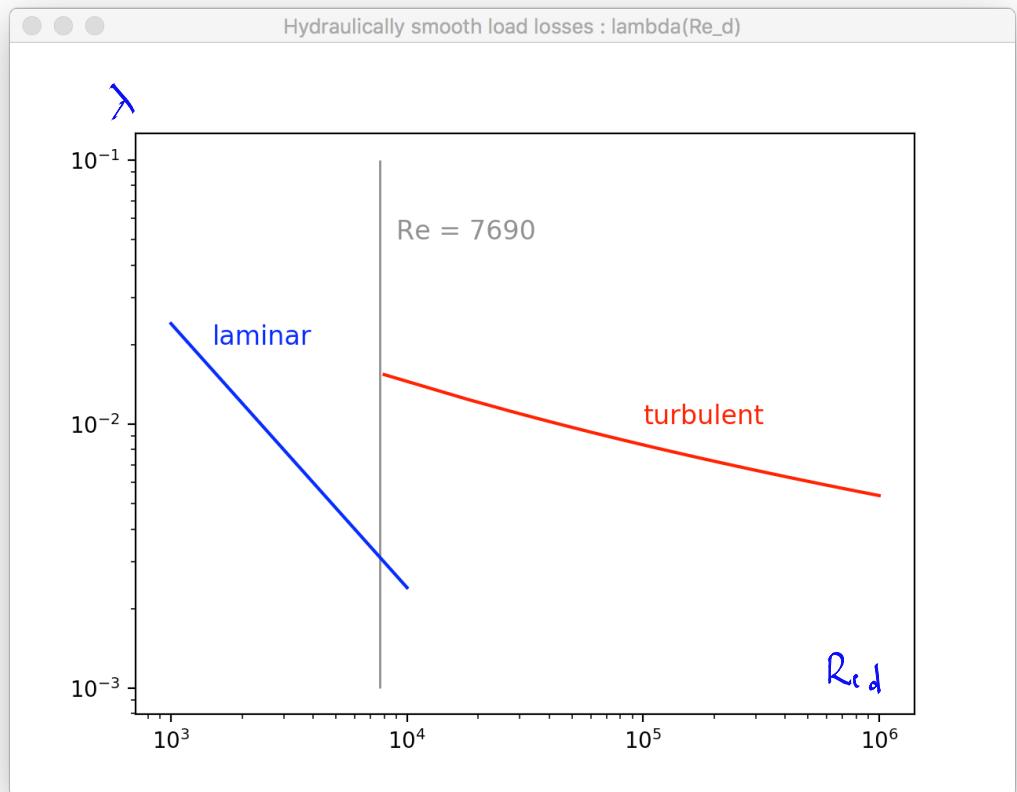
$$\frac{1}{2} \frac{2h \bar{v}_m}{\alpha} \frac{\bar{v}_c}{\bar{v}_m} = \frac{1}{2} R_{ed} \frac{\sqrt{x}}{2}$$

$$\frac{2}{\sqrt{x}} = -\frac{1}{\alpha} \log \left[\frac{u}{R_{ed}} \frac{1}{\sqrt{x}} \right] + \frac{1}{\alpha} \log \left[\exp(x [?]) \right]$$

$$\frac{1}{\sqrt{x}} = -\underbrace{\frac{2}{\alpha}}_a \underbrace{\frac{1}{\log_{10}(e)}}_b \log_{10} \left[\underbrace{\frac{u}{\exp(x [?])}}_b \frac{1}{\sqrt{x}} \right]$$

Utilisation de la formule implicite de Prandtl

$$\frac{1}{\sqrt{\lambda}} = -a \log_{10} \left(\frac{b}{Re_d} \frac{1}{\sqrt{\lambda}} \right)$$



```

Re_d = 10000 : lambda = 1.447e-02
Re_d = 100000 : lambda = 8.337e-03
Re_d = 1000000 : lambda = 5.358e-03

```

Hydraulically smooth load losses : lambda(Re_d)

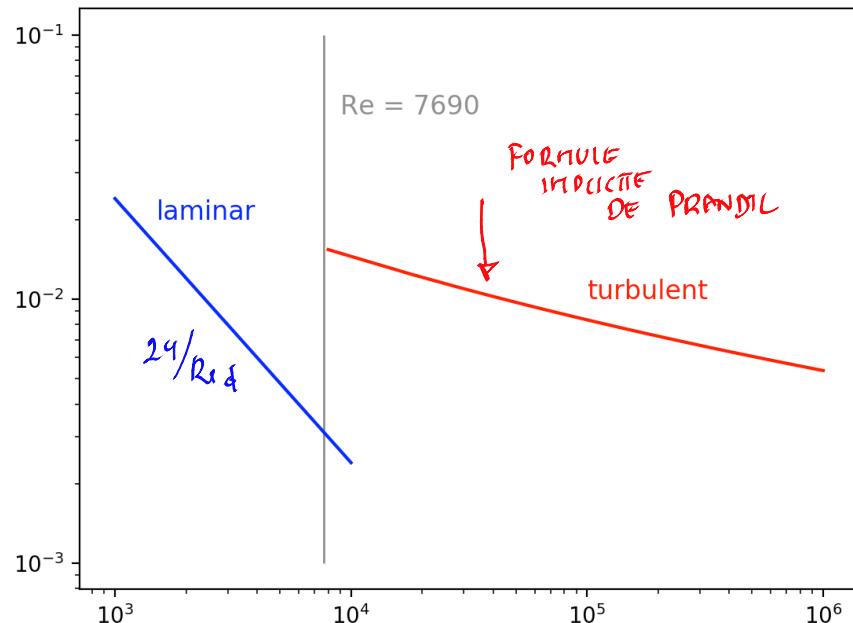
$$\frac{1}{\sqrt{\lambda}} = 1,778 \cdot Re^{1/8}$$

```

def computeLambda(Re) :
    delta = 100; i = 0
    xi = 1.778 * Re**(1/8)
    while delta > 1e-4 and i < 1000:
        old = xi
        xi = a*np.log10(xi*b/Re)
        delta = np.abs(old-xi); i = i+1
    return 1/(xi*xi)

for Re in [1e4,1e5,1e6] :
    print( " Re_d = %8d : lambda = %10.3e " % (Re,computeLambda(Re)) )

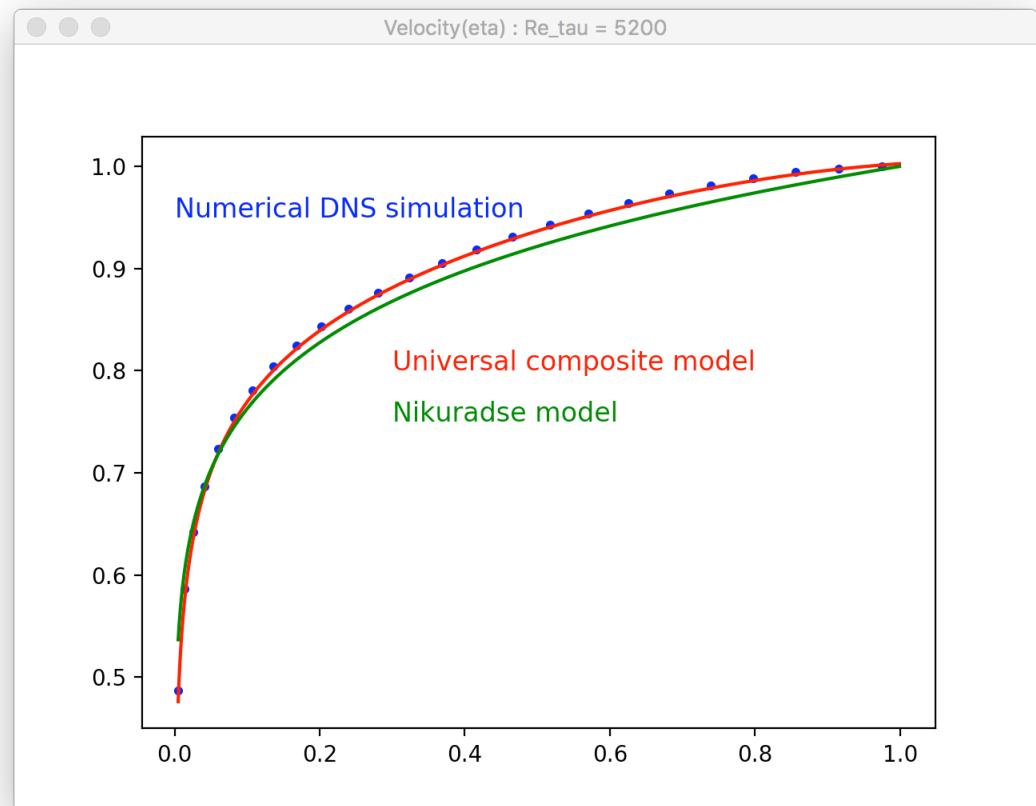
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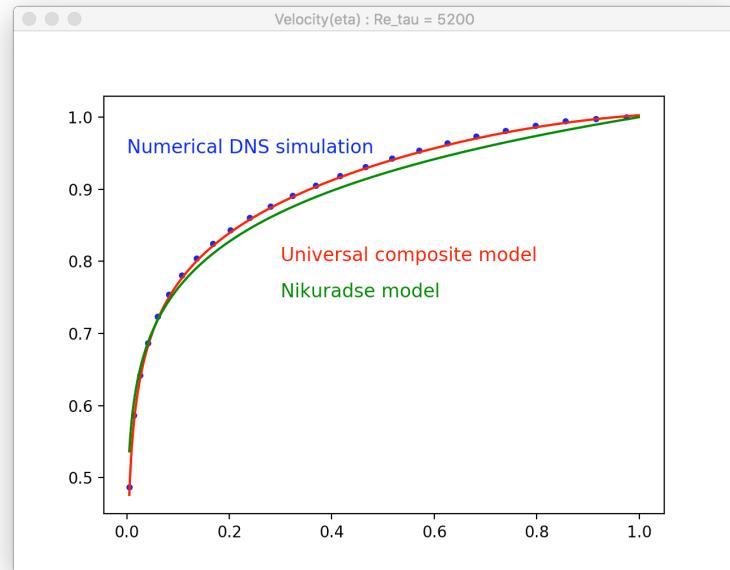
Nikuradse

Un bidouilleur de génie

$$\bar{v}(y) = \bar{v}_c \left[\frac{y}{h} \right]^{1/n}$$



Intégrales du déficit de vitesse



$$\boxed{1} \quad \bar{v}_m = \bar{v}_c \int_0^1 \eta^\alpha d\eta = \bar{v}_c \frac{1}{\alpha+1} \left[\frac{\eta^{\alpha+1}}{\alpha+1} \right]_0^1$$

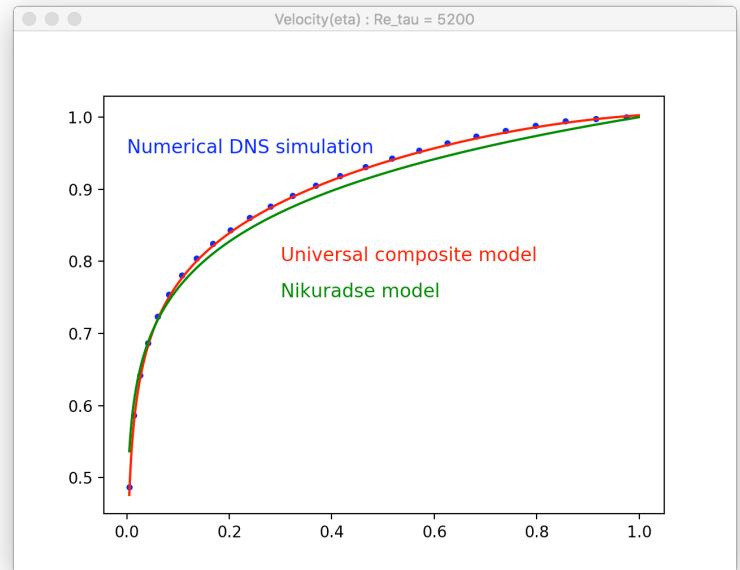
$\alpha = 1/m$

$$\boxed{\bar{v}_m = \bar{v}_c \frac{m}{m+1}}$$

$$\boxed{\int_0^1 \bar{v}_c - \bar{v}(\eta) d\eta = \bar{v}_c - \bar{v}_c \frac{m}{m+1} = \bar{v}_c \left[\frac{m+1-m}{m+1} \right] = \bar{v}_c \frac{1}{m+1}}$$

$$I_{Nik} = \int_0^1 \frac{\bar{v}_c - \bar{v}(\eta)}{\bar{v}_c} d\eta = \frac{1}{\bar{v}_m} \cancel{\frac{1}{\bar{v}_c}} \cancel{\frac{1}{m+1}} \cancel{\frac{\bar{v}_m}{\bar{v}_c}} \cancel{\frac{1}{m}} \cancel{\frac{1}{\bar{v}_c}} = \frac{1}{m} \frac{1}{\sqrt{\lambda}}$$

Nikuradse



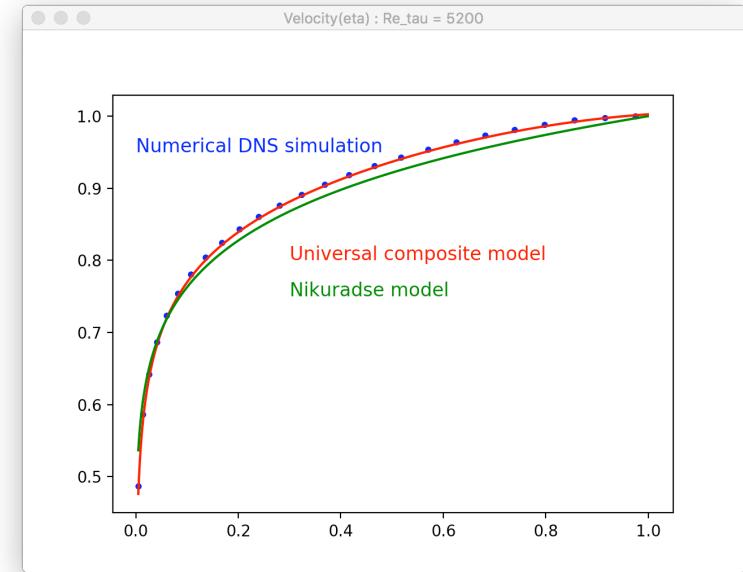
$$I_{Nik} = \frac{1}{n} \sqrt[2]{\lambda}$$



Composite

$$D[3\alpha^2 - 2\alpha^3]$$

$$\frac{\bar{v}_c - \bar{v}(\eta)}{\bar{v}_c} = \underbrace{\frac{1}{\delta e} \log \left[\frac{h \bar{v}_c}{\eta} \right]}_{-\frac{1}{\delta e} \log \left[\frac{y \bar{v}_c}{\eta} \right]} + \overbrace{G(1)}^{\sim} - \underbrace{\frac{1}{\delta e} \log \left[\frac{y}{h} \right]}_{-\frac{1}{\delta e} \log \left[\frac{y}{\eta} \right]} - G(\eta)$$



$$-D[3\alpha^2\eta^2 - 2\alpha^3\eta^3]$$

$$I_{Coles} = -\frac{1}{\delta e} \int_0^1 \log(\eta) d\eta + D \left[3\alpha^2\eta - 2\alpha^3\eta - \frac{3\alpha^2\eta^3}{3} - \frac{2\alpha^3\eta^4}{4} \right]_0^1$$

≈ -1

$$2\alpha^2 - 3\alpha^3/2 = 0$$

$$CAR \quad \alpha = 4/3$$

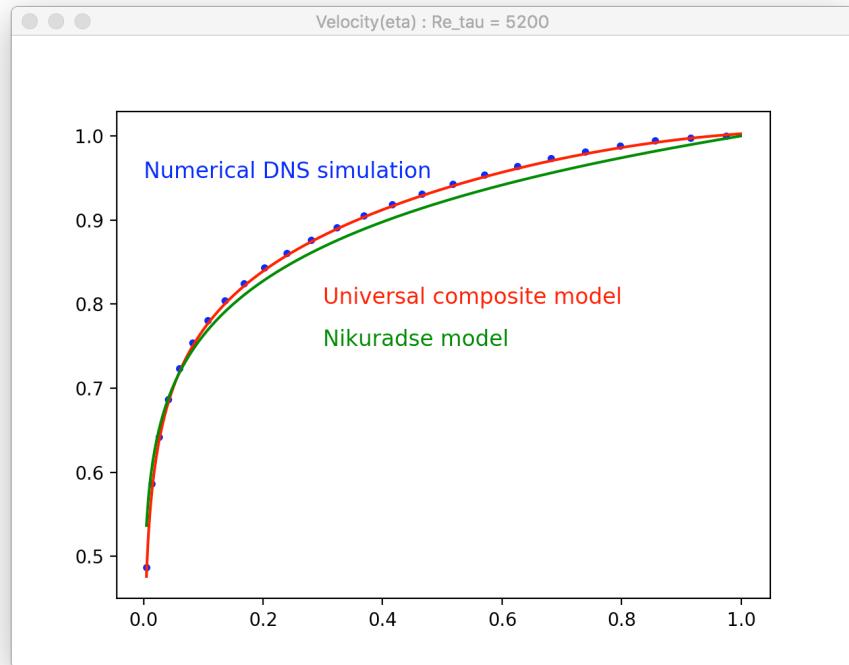
$$I_{Coles} = \frac{1}{\delta e}$$

Trouver le bon exposant !

$$n = \sqrt[2]{\frac{\delta e}{\lambda}}$$

$$I_{\text{COLES}} = \frac{1}{\delta e}$$

$$I_{\text{Nik}} = \frac{1}{n} \sqrt[2]{x}$$



```
Profil logarithmique ===== kappa = 0.3840 et C = 4.1500
Correction de Coles ===== alpha = 1.3333 et D = 0.3700
Nikuradse exponent ===== 1/n = 0.1177
Nikuradse exponent ===== n = 8.4958
Formule implicite de Prandtl = a = -2.9982 et b = 2.0309
```

Mais, c'est pas aussi joli
que le profil universel

