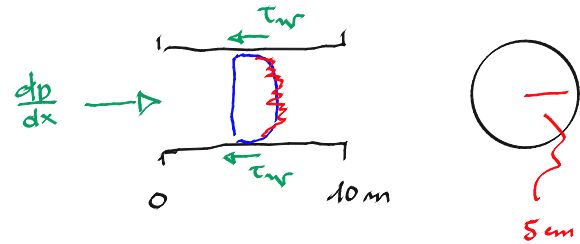
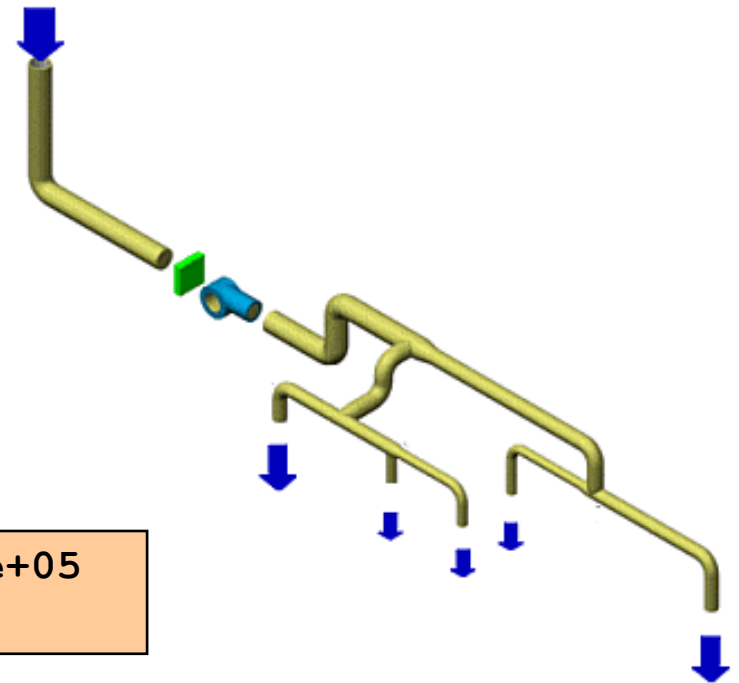


Ils savent même pas calculer
les pertes de charges
dans un tuyau !



$Re = 1.67e+05$



De l'air...

PRESSION

$$p = \frac{p}{R_* T}$$

101325 [Pa]

293 [K]

R/M

8.314 2,99 10⁻²

287,1 [J/kg K]

$$\rho = 1,204 \text{ [kg/m}^3\text{]}$$

$$\nu = \frac{\mu}{\rho} = 1,5 \cdot 10^{-5} \text{ [m}^2\text{/s]}$$



**Propriétés matérielles de l'air
à pression atmosphérique
et à une température de 20° Celsius**

μ	$1.81 \cdot 10^{-5}$	$N \cdot s \cdot m^{-2}$
k	$2.57 \cdot 10^{-2}$	$W \cdot m^{-1} \cdot K^{-1}$
c_p	$1.00 \cdot 10^3$	$J \cdot kg^{-1} \cdot K^{-1}$
M	$2.90 \cdot 10^{-2}$	$kg \cdot mole^{-1}$
R	8.314	$J \cdot mole^{-1} \cdot K^{-1}$

Estimer le problème !

$$Re = \frac{\bar{v}_m D}{\nu} = \frac{50 \text{ m/s} \cdot 5 \cdot 10^{-2} \text{ m}}{1,5 \cdot 10^{-5} \text{ m}^2/\text{s}} = 166\,609 \approx 1,7 \cdot 10^5$$

TURBULENT !

$$Ma = \frac{\bar{v}_m}{\sqrt{\gamma R_* \bar{T}_m}} = 0,14$$

LES EFFETS
COMPRESSIBLES
SEMBLENT MODESTES

$$Pr = \frac{\nu}{\alpha} = \frac{\mu c_p}{k} = 0,7$$

$$Ec = \frac{\bar{v}_m^2}{c_p (\bar{T}_m - \bar{T}_w)} = 0,25$$

20°C / 10°C

$$Ec = 0,25 \ll 1$$

$$Ec Pr = 0,176$$

DISSIPATION
VISQUEUSE
FAIBLE MAIS
PAS
TOTALLEMENT
NEGIGEABLE

nu	=	1.50e-05	[m2/s]
rho	=	1.21e+00	[kg/m3]
Re	=	1.67e+05	
Pr	=	7.04e-01	
Ec	=	2.50e-01	
Ec Pr	=	1.76e-01	
Ma	=	1.46e-01	



Nusselt

$$Nu = \frac{q_w}{k \Delta T / D}$$

$$\frac{\rho D \bar{u}_m}{\mu} \quad \frac{\mu c_p}{k}$$

St

$$Pe = Re Pr$$

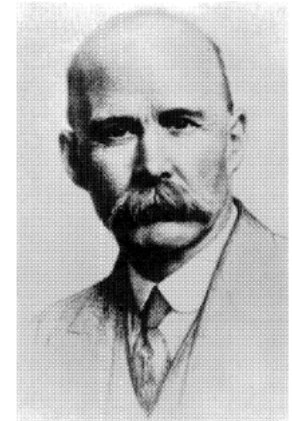
$$Nu = \frac{q_w D}{k \cancel{\Delta T}} \frac{\rho c \bar{u}_m \cancel{\Delta T}}{\rho c \bar{u}_m \Delta T} = \frac{q_w}{\rho c \bar{u}_m \Delta T}$$

$$\frac{D \bar{u}_m \rho c}{k}$$

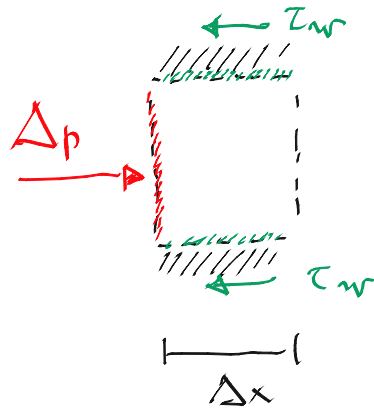
$$Nu = St Re Pr$$

$$St = \frac{q_w}{\rho c \bar{u}_m \Delta T}$$

Stanton



Faire avancer un fluide dans un tuyau !



$$\Delta p / \pi R^2 = \tau_w 2\pi R \Delta x$$

$$2 \tau_w = \frac{dp}{dx}$$

$$C_f = \frac{\tau_w}{\rho \bar{v}_m^2 / 2}$$
$$\lambda = \frac{dp/dx}{\rho \bar{v}_m / D}$$

$$4 C_f = \lambda$$



Tuyau lisse

$$\frac{1}{\sqrt{\lambda}} = -2 \log_{10} \left(\frac{2.51}{Re_D} \frac{1}{\sqrt{\lambda}} + \frac{1}{3.71} \frac{\epsilon}{2R} \right)$$

$$St = \frac{\lambda}{8} \left(1 + 13 \left(Pr^{2/3} - 1 \right) \sqrt{\frac{\lambda}{8}} \right)^{-1}$$

$\epsilon = 0$

$$\lambda = 1,61 \cdot 10^{-2}$$

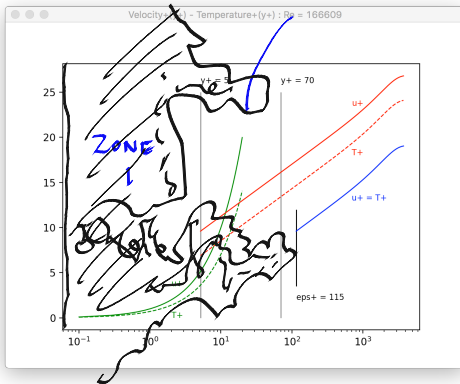
$$St = 2,31 \cdot 10^{-3}$$

==== Smooth pipe =====

Lambda	=	1.621e-02
St	=	2.308e-03
Nu	=	2.708e+02
Pressure difference	=	4.889e-01 [bar]
Pressure gradient	=	4.889e-03 [bar/m]
Heat flux density	=	1.392e+03 [Watt/m2]
Heat transfer coeff	=	1.392e+02 [Watt/m2K]

Tuyau rugueux

ZONE II



$$\frac{1}{\sqrt{\lambda}} = -2 \log_{10} \left(\frac{2.51}{Re_D} \frac{1}{\sqrt{\lambda}} + \frac{1}{3.71} \frac{\epsilon}{2R} \right)$$

$\epsilon = 1/2 \text{ mm}$

$$St = \frac{\lambda}{8} \left(1 + 13 \left(Pr^{2/3} - 1 \right) \sqrt{\frac{\lambda}{8}} \right)^{-1}$$

$$\lambda = 3,82 \cdot 10^{-2}$$

$$St = \frac{\lambda}{8} = 4,78 \cdot 10^{-3}$$

$$\epsilon^+ = 115$$

==== Rough pipe === epsilon = 5.00e-04 =====

Epsilon_+	=	1.152e+02	
Lambda	=	3.823e-02	
St	=	4.779e-03	
Nu	=	5.608e+02	
Pressure difference	=	1.153e+00	[bar]
Pressure gradient	=	1.153e-02	[bar/m]
Heat flux density	=	2.882e+03	[Watt/m2]
Heat transfer coeff	=	2.882e+02	[Watt/m2K]

Laminaire virtuel

$$\lambda = \frac{64}{Re} = 3,84 \cdot 10^{-4}$$

$$St = 6,07 \cdot 10^{-5}$$

$$Nu = 7,12$$

SUMMARY :-)

	TURBULENT RUGUEUX	TURB LISSE	LAMINAIRE
λ	$4 \cdot 10^{-2}$	$2 \cdot 10^{-2}$	$4 \cdot 10^{-4}$
Nu	561	271	3... 9

$$Nu = 9,6 \dots 3,66$$

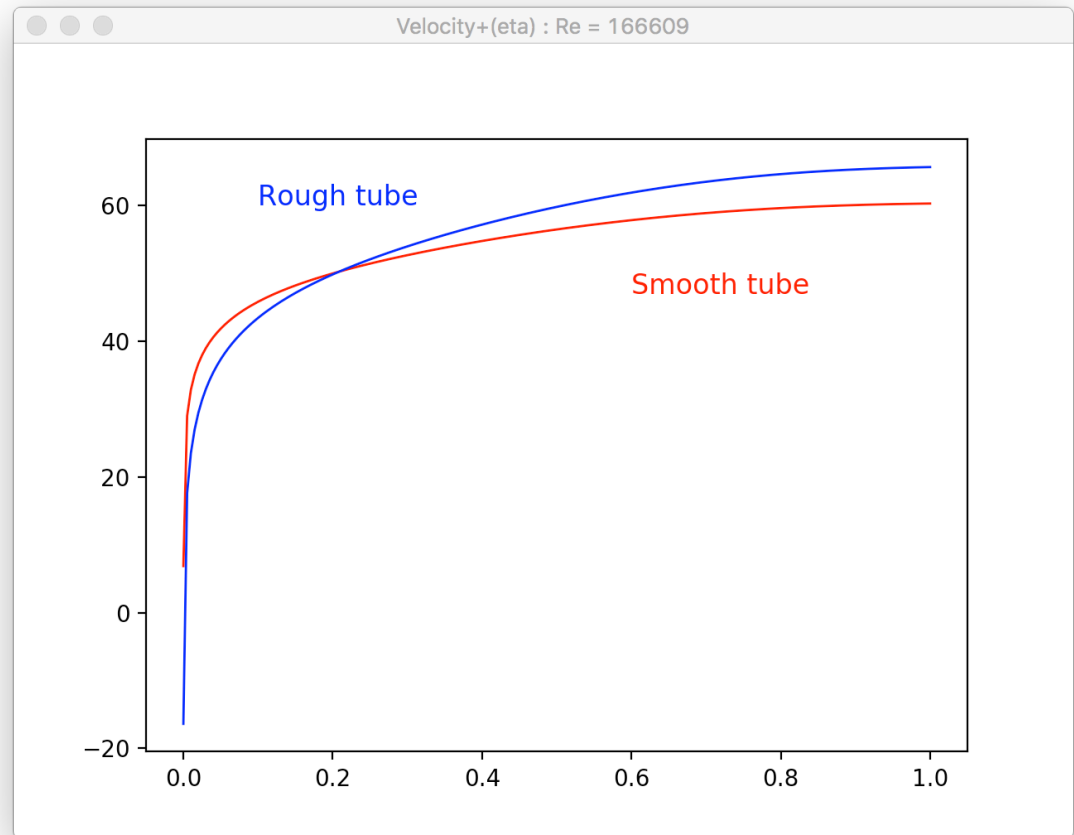


C'EST
LE PRIX
A PAYER

```

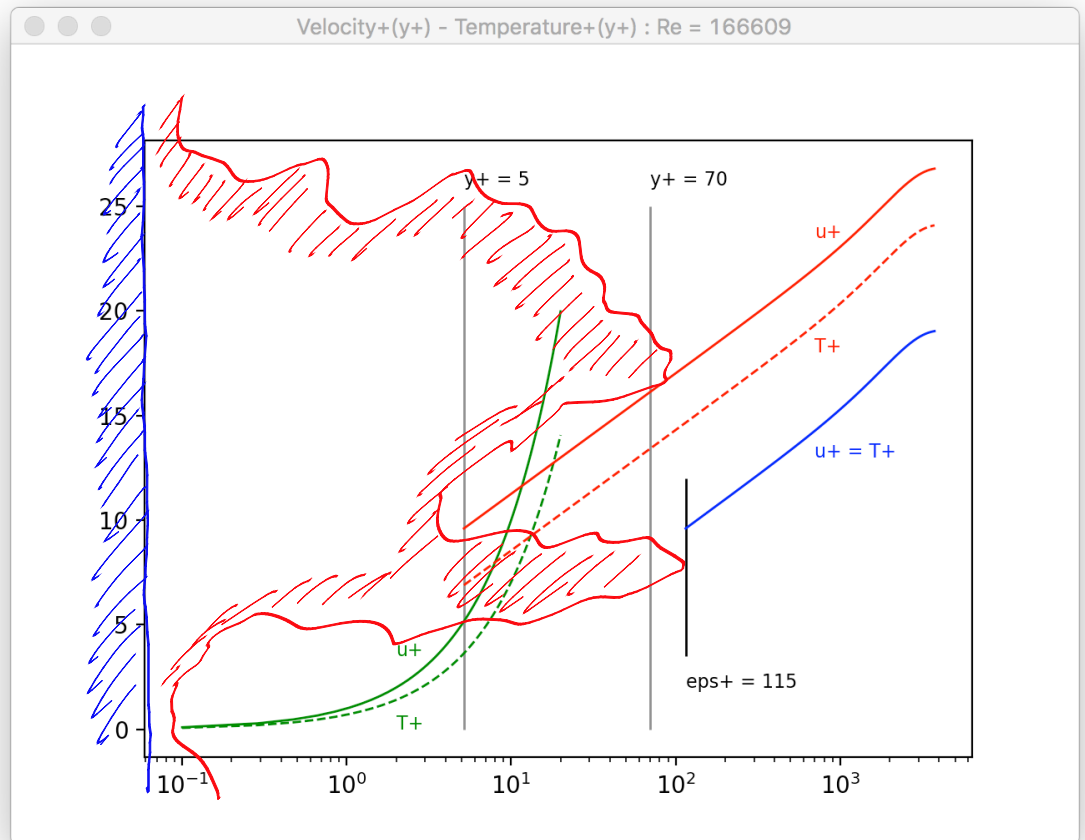
===== Virtual laminar pipe =====
Epsilon_+          = 1.152e+02
Lambda             = 3.841e-04
St                 = 6.066e-05
Nu                 = 7.118e+00
Pressure difference = 1.158e-02 [bar]
Pressure gradient  = 1.158e-04 [bar/m]
Heat flux density  = 3.658e+01 [Watt/m2]
Heat transfer coeff = 3.658e+00 [Watt/m2K]
    
```


Dessiner le problème



```
==== Profil logarithmique ===== kappa = 0.4000 et C = 5.5000
==== Correction de Coles ===== alpha = 1.3500 et D = 1.0000
==== Approximated mean velocity (smooth) : 54.3 [m/s]
==== Approximated mean velocity (rough) : 56.4 [m/s]
```

Près de la paroi...



$$Pr_{turb} = 1$$

$$0 = \frac{d}{dy} (\bar{v} + \bar{v}^t)$$

$$\bar{v}(y) + \bar{v}^t(y) = \bar{v}_w (1 - y/R)$$

$$= -k \frac{dT}{dy} \quad = -k^t \frac{dT}{dy}$$

ZONE
A DOMINANCE
LAMINAIRE

$$-\alpha \frac{dT}{dy} - \alpha^t \frac{dT}{dy} = \frac{\bar{v}_w}{\rho c} (1 - y/R)$$

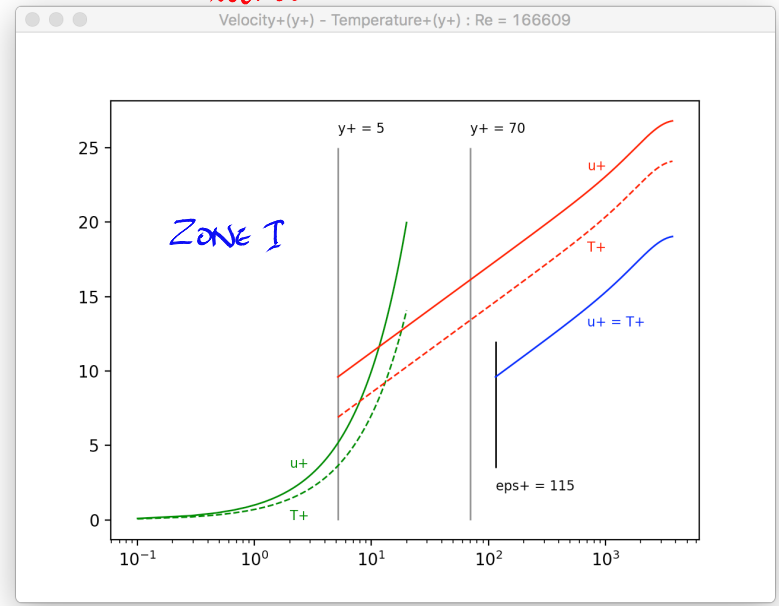
NEGLIGE

$$y/R \ll 1$$

$$\bar{T}_w - \bar{T}(y) = \frac{1}{\alpha \rho c} \bar{v}_w y$$

$$= \frac{U}{\alpha} \frac{\bar{v}_w}{\rho c \sigma_c} \frac{\sigma_c y}{U}$$

$$\bar{T}^+ = Pr y^+ = Pr \sigma^+$$



$$Pr_{turb} = 1$$

$$-\alpha \frac{d\bar{T}}{dy} - \alpha^t \frac{d\bar{T}}{dy} = \frac{\bar{q}_w}{\rho c} (1 - y/R)$$

NEGLIGE

$1st(y)$

ZONE A DOMINANCE TURBULENCE

$$1st(y) \frac{d\bar{T}}{dy} = \frac{\bar{q}_w}{\rho c} (1 - \frac{y}{R})$$

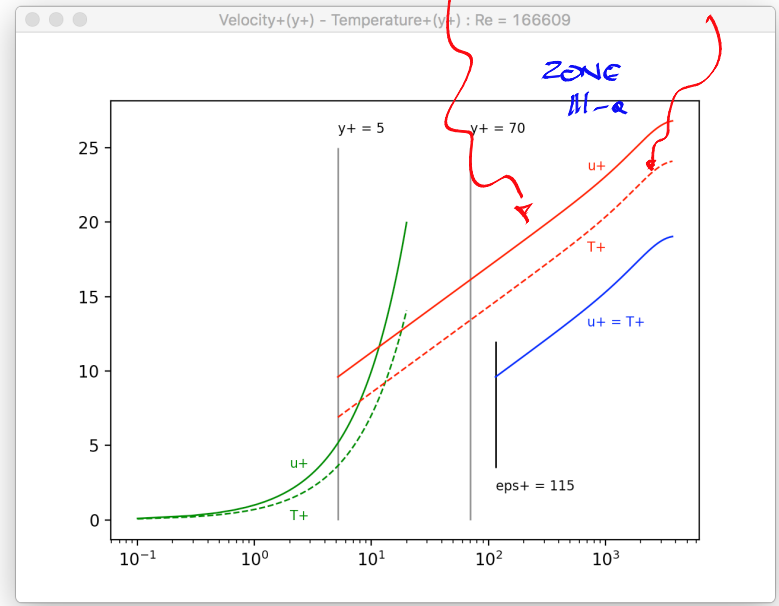
$\propto y \bar{u}_t (1 - y/R)$

$$\bar{T}^+ = \frac{1}{\kappa} \log(\bar{y}^+) + A$$

FUNCTION DE Pr :-)

CAS RUGUEUX

$$\bar{T}^+ = \frac{1}{\kappa} \log\left(\frac{y}{\epsilon}\right) + B$$



Est-ce un modèle réaliste ?

$$p = \frac{\rho}{RT}$$

