

$$\frac{\delta^*}{\delta} = \frac{L}{\delta} \int_0^{\delta} \left(1 - \frac{\bar{u}}{\bar{u}_e}\right) dy = \frac{\bar{u}_e}{\bar{u}_e} \frac{L}{\delta} \int_0^{\delta} \left(\frac{\bar{u}_e - \bar{u}}{\bar{u}_e}\right) dy$$

$$= \frac{\bar{u}_e}{\bar{u}_e} \frac{L}{\delta} \int_0^1 F(\eta) d\eta$$

zone III est dominante!

$\frac{L}{\delta} \approx \sqrt{\frac{CF}{2}}$
III
 $a \approx 3.4$

$$\frac{(\delta^* - \theta)}{\delta} = \frac{L}{\delta} \int_0^{\delta} \left(1 - \frac{\bar{u}}{\bar{u}_e}\right)^2 dy = \frac{\bar{u}_e^2}{\bar{u}_e^2} \int_0^1 (F(\eta))^2 d\eta$$

$\frac{L}{\delta} \approx \sqrt{\frac{CF}{2}}$
III
 $b \approx 2.3$

Notation $\eta = \frac{y}{\delta} = \sqrt{\frac{2}{CF}}$

$\hookrightarrow \frac{\delta^*}{\delta} = \frac{a}{\eta}$

et $\frac{(\delta^* - \theta)}{\delta} = \frac{b}{\eta^2} \implies \frac{\theta}{\delta} = \frac{a}{\eta} - \frac{b}{\eta^2}$

Aussi $H = \frac{\delta^*}{\theta} = \text{facteur de forme}$

$\hookrightarrow H = \frac{\frac{a}{\eta}}{\left(\frac{a}{\eta} - \frac{b}{\eta^2}\right)} = \frac{1}{\left(1 - \frac{b}{a} \frac{1}{\eta}\right)}$

Profils simplifiés en exposant

$$\frac{\bar{v}}{v_0} = \eta^{1/m}$$

$$\hookrightarrow \frac{S^*}{S} = \int_0^1 (1 - \eta^{1/m}) d\eta = \frac{1}{(m+1)}$$

$$\text{et } \frac{(S^* - \theta)}{S} = \int_0^1 (1 - \eta^{1/m})^2 d\eta = \int_0^1 (1 - 2\eta^{1/m} + \eta^{2/m}) d\eta = \frac{2}{(m+1)(m+2)}$$

$$\hookrightarrow \frac{\theta}{S} = \frac{1}{(m+1)} - \frac{2}{(m+1)(m+2)} = \frac{m}{(m+1)(m+2)}$$

$$\hookrightarrow H = \frac{(m+2)}{m}$$

Comparaison

$$\frac{(m+2)}{m} \approx \frac{1}{\left(1 - \frac{1}{a} \frac{1}{\beta}\right)}$$

$$\text{III} \\ \frac{(m+2)}{(m+2)-2}$$

$$\text{III} \\ \frac{1}{\left(1 - \frac{2}{(m+2)}\right)}$$

$$\hookrightarrow \frac{2}{(m+2)} \approx \frac{1}{a} \frac{1}{\beta}$$

\Leftrightarrow

$m \approx 2 \left(\frac{a}{\beta} \beta - 1 \right)$
$m \approx 2 (0.15 \beta - 1)$

Simple et utile !

Cas russe

$$\frac{\bar{v}}{\bar{v}_e} = \left(\frac{1}{K} \log \left(\frac{y \bar{v}_e}{\bar{v}} \right) + C \right) + G \left(\frac{y}{\delta} \right)$$

$$\hookrightarrow \frac{\bar{v}_e}{\bar{v}_e} = \left(\frac{1}{K} \log \left(\frac{\delta \bar{v}_e}{\bar{v}_e} \right) + C \right) + G(1)$$

$$\frac{\delta \bar{v}_e}{\bar{v}_e}$$

$$\hookrightarrow \boxed{\bar{v}_3 = \frac{1}{K} \log \left(\text{Res} \frac{1}{\bar{v}_3} \right) + C + G(1)} = \text{exact (mais implicite)}$$

• Approximation de White: $\bar{v}_3 \approx 10 \text{ Res}^{1/2}$

$$\hookrightarrow \frac{d\theta}{dx} = \frac{1}{\bar{v}_3^2} \approx \frac{1}{100} \left(\frac{\delta \bar{v}_e}{\bar{v}_e} \right)^{1/6}$$

• Approximation: négliger la variation de $\frac{\theta}{\delta}$

et prendre la valeur pour $n=7$

$$\hookrightarrow \frac{\theta}{\delta} \approx \frac{7}{8 \times 9} = \frac{7}{72} \approx 0.0972$$

$$\hookrightarrow \frac{7}{72} \times 100 \frac{d\delta}{dx} \approx \frac{1}{\left(\frac{\delta \bar{v}_e}{\bar{v}_e} \right)^{1/6}}$$

$$\delta^{1/6} d\delta \approx \frac{72}{700} \left(\frac{\bar{v}_e}{\delta} \right)^{1/6} dx$$

$$\frac{\delta^{7/6}}{7/6} \approx \frac{72}{700} \left(\frac{\bar{v}_e}{\delta} \right)^{1/6} x$$

$$\delta \approx \left(\frac{12}{100} \right)^{6/7} \frac{x^{6/7}}{\left(\frac{\bar{v}_e}{\delta} \right)^{1/7}} \Rightarrow \frac{\delta}{x} \approx \frac{0.162}{\left(\frac{\bar{v}_e x}{\delta} \right)^{1/7}}$$

$$\frac{\delta}{x} \approx \frac{0.162}{R_{ex}^{1/7}}$$

$$\text{avec } R_{ex} \triangleq \frac{\bar{v} x}{\nu}$$

$$\hookrightarrow \frac{\theta}{x} \approx \frac{0.0158}{R_{ex}^{1/7}} \quad \longrightarrow \quad C_f = 2 \frac{d\theta}{dx} \approx \frac{0.0371}{R_{ex}^{1/7}}$$

$$\text{et } \frac{\delta^*}{x} \approx \frac{0.0203}{R_{ex}^{1/7}} \quad \hookrightarrow \quad C_{f,m} = \frac{2\theta}{x} \approx \frac{0.0316}{R_{ex}^{1/7}}$$

Analyse plus précise de White (1962)

$$\hookrightarrow \dots \longrightarrow C_f \approx \frac{0.455}{(\log(0.060 R_{ex}))^2}$$

$$C_{f,m} \approx \frac{0.523}{(\log(0.060 R_{ex}))^2}$$

Formule de Schultz-Grunow

$$C_f \approx \frac{0.37}{(\log_{10}(R_{ex}))^{2.584}}$$

Note:

$$\eta_3 = \frac{1}{K} \log(\text{Res}_0 \frac{1}{\eta_3}) + C + G(1)$$

$$= \frac{1}{K} \log(\text{Res}_0 \frac{c}{\eta_3}) \quad \text{avec } c = e^{K(C+G(1))}$$

$$\hookrightarrow K\eta_3 = \log(\text{Res}_0 \frac{c}{\eta_3})$$

$$\hookrightarrow \boxed{\text{Res}_0 = \frac{\eta_3}{c} e^{K\eta_3}} \quad \equiv \text{exact et explicite!}$$

Aussi $\frac{\theta}{\delta} = \frac{a}{\eta_3} - \frac{b}{\eta_3^2} \quad \equiv \text{exact}$

$$\hookrightarrow \theta = \left(\frac{a}{\eta_3} - \frac{b}{\eta_3^2} \right) \delta \quad \Rightarrow \quad \boxed{\text{Res}_0 = \left(\frac{a}{\eta_3} - \frac{b}{\eta_3^2} \right) \text{Res}}$$

$$\hookrightarrow \text{Res}_0 = \left(\frac{a}{\eta_3} - \frac{b}{\eta_3^2} \right) \frac{\eta_3}{c} e^{K\eta_3}$$

$$\boxed{\text{Res}_0 = \frac{1}{c} \left(a - \frac{b}{\eta_3} \right) e^{K\eta_3}} \quad \equiv \text{exact}$$

$$\frac{d\theta}{dx} = \frac{d(\text{Res}_0)}{d(\text{Res}_x)} = \frac{1}{\eta_3^2} \quad \Rightarrow \quad \boxed{\eta_3^2 d(\text{Res}_0) = d(\text{Res}_x)} \quad \equiv \text{exact}$$

$$\hookrightarrow \boxed{\frac{\eta_3^2}{c} d\left(\left(a - \frac{b}{\eta_3} \right) e^{K\eta_3} \right) = d\text{Res}_x} \quad \equiv \text{exact}$$

\hookrightarrow Intégrer. On obtient Res_x en fonction de η_3
(voir syllabus)

Cas rugueux

$$\frac{\bar{U}}{\bar{U}_r} = \left(\frac{1}{K} \log\left(\frac{y}{E}\right) + B \right) + G\left(\frac{y}{E}\right)$$

$$\hookrightarrow \frac{\bar{U}_e}{\bar{U}_r} = \frac{1}{K} \log\left(\frac{\delta}{E}\right) + B + G(1)$$

$$= \frac{1}{K} \log\left(\frac{\delta}{E} C_2\right) \quad \text{avec} \quad C_2 = e^{K(B+G(1))}$$

$$\hookrightarrow \boxed{\eta_3 = \frac{1}{K} \log\left(\frac{\delta}{E} C_2\right)} \quad \equiv \text{exact et explicite}$$

$$\hookrightarrow \boxed{\frac{\delta}{E} = \frac{1}{C_2} e^{K\eta_3}} \quad \equiv \text{exact et explicite}$$

$$\hookrightarrow \frac{d\theta}{dx} = \frac{1}{\eta_3^2} = \frac{K^2}{\log^2\left(\frac{\delta}{E} C_2\right)}$$

On obtient $\frac{x}{E}$ en fonction

\hookrightarrow etc... voir syllabus de $\frac{\delta}{E}$, et donc aussi $\frac{x}{E}$ en fonction de η_3

Formules empiriques de Schlichting (1979)

$$C_f \approx \frac{1}{\left(2.87 + 1.58 \log_{10}\left(\frac{x}{E}\right)\right)^{2.5}}$$

$$C_{f,m} \approx \frac{1}{\left(1.89 + 1.62 \log_{10}\left(\frac{x}{E}\right)\right)^{2.5}}$$

Formule de White

$$C_f \approx \frac{1}{\left(1.4 + 3.7 \log_{10}\left(\frac{x}{E}\right)\right)^2}$$

Transfert de chaleur en couches limites

$$\rho c \left(\frac{\partial T}{\partial t} + \frac{\partial (T v_j)}{\partial x_j} \right) = \tau_{ij} d_{ij} - \frac{\partial q_j}{\partial x_j} \quad \text{avec } \left. \begin{array}{l} \tau_{ij} = \mu d_{ij} \\ q_j = -k \frac{\partial T}{\partial x_j} \end{array} \right\}$$

$$= \mu d_{ij} d_{ij} + \frac{\partial}{\partial x_j} \left(k \frac{\partial T}{\partial x_j} \right)$$

Moyenne de Reynolds

$$\overline{TV_j} = \bar{T} \bar{v}_j + \overline{T'v_j'}$$

$$\overline{d_{ij}d_{ij}} = \overline{d_{ij}d_{ij}} + \overline{d_{ij}'d_{ij}'}$$

$$\hookrightarrow \rho c \frac{\partial (\bar{T} \bar{v}_j)}{\partial x_j} = \mu (\overline{d_{ij}d_{ij}} + \overline{d_{ij}'d_{ij}'}) + \frac{\partial}{\partial x_j} \left(k \frac{\partial \bar{T}}{\partial x_j} - \rho c \overline{T'v_j'} \right)$$

$$\hookrightarrow \bar{q}_j = -k \frac{\partial \bar{T}}{\partial x_j}$$

$$\bar{q}_j^t \triangleq \rho c \overline{T'v_j'} \quad \text{= densité de flux de chaleur due aux fluctuations de la turbulence}$$

Modèle: $\bar{q}_j^t = -k_t \frac{\partial \bar{T}}{\partial x_j}$

$$\mu d_{ij} d_{ij} \approx \mu_t d_{ij} d_{ij} \quad (\mu_k \text{ pour écoulements turbulents simples})$$

Couche limite: $\bar{q}_j^t = \rho c \overline{T'v_j'} = -k_t \frac{\partial \bar{T}}{\partial x_j}$

$$\rho c (\bar{u} \frac{\partial \bar{T}}{\partial x} + \bar{v} \frac{\partial \bar{T}}{\partial y}) = (\mu + \mu_t) \left(\frac{\partial \bar{u}}{\partial y} \right)^2 + \frac{\partial}{\partial y} \left((k + k_t) \frac{\partial \bar{T}}{\partial y} \right)$$

car $\frac{\partial}{\partial x} \left((k + k_t) \frac{\partial \bar{T}}{\partial x} \right)$ est négligeable

$$T_2 \triangleq \frac{\mu c}{k} = \frac{v}{\alpha} \quad \text{car } \begin{cases} v \triangleq \frac{\mu}{\rho} \\ \alpha \triangleq \frac{k}{\rho c} \end{cases}$$

$$T_{2t} \triangleq \frac{\mu_t c}{k_t} = \frac{v_t}{\alpha_t} \quad \text{car } \begin{cases} v_t = \frac{\mu_t}{\rho} \\ \alpha_t = \frac{k_t}{\rho c} \end{cases}$$

Pour la suite, on va supposer que T_{2t} est constant

$$(0) \quad \frac{\partial \bar{u}}{\partial x} + \frac{\partial \bar{v}}{\partial y} = 0$$

on considère \bar{u}_e constant

$$(1) \quad \rho \left(\bar{u} \frac{\partial \bar{u}}{\partial x} + \bar{v} \frac{\partial \bar{u}}{\partial y} \right) = \rho \bar{u}_e \frac{d\bar{u}_e}{dx} + \frac{\partial}{\partial y} \left((\mu + \mu_t) \frac{\partial \bar{u}}{\partial y} \right)$$

$$(2) \quad \rho c \left(\bar{u} \frac{\partial \bar{T}}{\partial x} + \bar{v} \frac{\partial \bar{T}}{\partial y} \right) = (\mu + \mu_t) \left(\frac{\partial \bar{u}}{\partial y} \right)^2 + \frac{\partial}{\partial y} \left(\left(\frac{\mu}{T_2} + \frac{\mu_t}{T_{2t}} \right) c \frac{\partial \bar{T}}{\partial y} \right)$$

$\bar{u} * \text{Eq. (1)} + \text{Eq. (2)}$:

$$\hookrightarrow \rho \left(\bar{u} \frac{\partial}{\partial x} \left(c\bar{T} + \frac{\bar{u}^2}{2} \right) + \bar{v} \frac{\partial}{\partial y} \left(c\bar{T} + \frac{\bar{u}^2}{2} \right) \right) = \frac{\partial}{\partial y} \left(\left(\frac{\mu}{T_2} + \frac{\mu_t}{T_{2t}} \right) \frac{\partial}{\partial y} \left(c\bar{T} + \frac{\bar{u}^2}{2} \right) \right)$$

Cas $T_2=1$ et $T_{2t}=1$

L'EST pour $(c\bar{T} + \frac{\bar{u}^2}{2})$ est idem que l'EST pour \bar{u}

\hookrightarrow les profils sont liés linéairement

$$\boxed{c\bar{T} + \frac{\bar{u}^2}{2} = A\bar{u} + B} \equiv \text{Relation de Crocco}$$

Rappel: $dU = c dT$

en $y=0$: $\bar{v}=0$ et $\bar{T}=\bar{T}_w \Rightarrow B = c\bar{T}_w$

en $y=\delta$: $\bar{v}=\bar{v}_e$ et $\bar{T}=\bar{T}_e \Rightarrow c\bar{T}_e + \frac{\bar{v}_e^2}{2} = A\bar{v}_e + B$
 $= A\bar{v}_e + c\bar{T}_w$

$\hookrightarrow A = \frac{1}{\bar{v}_e} \left(c(\bar{T}_e - \bar{T}_w) + \frac{\bar{v}_e^2}{2} \right)$

$\hookrightarrow c(\bar{T} - \bar{T}_w) + \frac{\bar{v}^2}{2} = \left(c(\bar{T}_e - \bar{T}_w) + \frac{\bar{v}_e^2}{2} \right) \frac{\bar{v}}{\bar{v}_e}$

Aussi $c \frac{\partial \bar{T}}{\partial y} + \bar{v} \frac{\partial \bar{v}}{\partial y} = A \frac{\partial \bar{v}}{\partial y}$

\hookrightarrow en $y=0$: $c \frac{\partial \bar{T}}{\partial y} \Big|_0 = A \frac{\partial \bar{v}}{\partial y} \Big|_0$

Cas lisse (Zone I) $T_{r2} = \frac{\mu c}{k} = 1 \Rightarrow c = \frac{k}{\mu}$

$\hookrightarrow k \frac{\partial \bar{T}}{\partial y} \Big|_0 = A \mu \frac{\partial \bar{v}}{\partial y} \Big|_0$

$\hookrightarrow -\bar{q}_w = A \bar{T}_w$

Cas rugueux (Zone III) $T_{r+} = \frac{\mu_+ c}{k_+} = 1 \Rightarrow c = \frac{k_+}{\mu_+}$

$\hookrightarrow k_+ \frac{\partial \bar{T}}{\partial y} \Big|_0 = A \mu_+ \frac{\partial \bar{v}}{\partial y} \Big|_0$

$\hookrightarrow -\bar{q}_w = A \bar{T}_w \equiv \text{idem!}$

Donc $A = -\frac{\bar{q}_w}{\bar{T}_w}$ dans tous les cas